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MULTICOLOR CCD PHOTOMETRY OF THE OPEN CLUSTER IC 361

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Abstract. GCD photometry in the eight-color Vilnius+I system for 7250 stars down to I=19.6 mag has been obtained in the $20'\times26'$ field of the open cluster IC 361 in Camelopardalis. The catalog of 1420 stars down to $V\sim18.5$ mag is presented. It contains the coordinates, V magnitudes and seven color indices, quantitative photometric spectral types, absolute magnitudes and distances. The interstellar extinction is found to be non-uniform across the field, with the values of A_V in the range 1.9 to 2.4 mag. The distribution of distance moduli of individual stars shows that the cluster is located as far as, or just beyond, the Perseus spiral arm.

Key words: stars: fundamental parameters – Galaxy: open clusters: individual (IC 361)

1. INTRODUCTION

The open cluster IC 361 in Camelopardalis ($\ell=147.5^{\circ}$, $b=5.7^{\circ}$) is well detached from the field, but because of faintness it has been very poorly studied. The only photometric information published to date is that by Piccirillo & Stein (1978) who obtained in the field of the cluster photoelectric UBV and photographic BV data for 19 and 32 stars, respectively, identified the contours of the main sequence and identified a few red giant stars. Based on these preliminary data they adopted a distance of 2.5 kpc, a high value of reddening, $E_{B-V}=0.55$, and suggested the age in the range 0.5 to 1 Gyr. IC 361 lies in the second Galactic quadrant, in the immediate vicinity of the Camelopardalis dark clouds. Therefore, it is not surprising that the cluster demonstrates a considerable interstellar reddening. In such a case, the contribution of multicolor medium-band photometry can provide improved determinations of the fundamental parameters of the cluster. For this purpose we have undertaken CCD observations in the *Vilnius* seven-color system in the $20' \times 20'$ field covering the cluster and its immediate surroundings. An I filter of the Cousins photometric system has been added.

In Section 2 we describe our observations in the field of IC 361 and data reduc-

tions. In Section 3 we present the results of photometry. The methods for quantitative classification of individual stars are described in Section 4. The derived spectral types, the values of interstellar extinction and distances to individual stars are given in Table 3. A brief discussion of the results is given in Section 5. The cluster parameters derived with these data will be presented in the forthcoming paper.

2. OBSERVATIONS AND REDUCTIONS

CCD observations in seven filters U,P,X,Y,Z,V,S of the Vilnius system plus the filter I of the Cousins system were carried out in December of 1999 with a 2K CCD camera on the 1 m telescope of the USNO Flagstaff Station (Arizona), which gives a field of the diameter of 20'. Repeated observations in the Vilnius filters were done with the same telescope and a new $2K \times 2K$ CCD camera in March of 2009. During the latter run we have obtained well-calibrated CCD data only for filters Y, Z, V, S, since observations through the remaining three filters on the succeeding night were curtailed by cirrus clouds.

Additional frames in the *Vilnius* filters U, Y, V were taken for the central part of the field $(12' \times 12')$ in December of 2008 with a 4K CCD camera on the 1.8 m Vatican Advanced Technology Telescope (VATT) on Mt. Graham (Arizona).

The exposures taken during the three observing runs are listed in Table 1. Since some exposures were done with a small shift in DEC, the measured field coverage is about $20' \times 26'$. Figure 1 shows a Flagstaff exposure in the I filter.

Table 1. CCD exposures taken with the Flagstaff 1 m telescope and the VATT.

Filter	λ_0 (nm)	Number of fra	mes × exposure tin	ne (in seconds)
		Flagstaff 1999	Flagstaff 2009	VATT 2008
U	345	2 × 1800		$3 \times 1500 \ 3 \times 150$
P	374	$2 \times 1800 \ 2 \times 300$		
X	405	$2 \times 1800 \ 2 \times 300$		
Y	466	$2 \times 360 2 \times 60$	$1 \times 720 2 \times 600$	$3 \times 200 3 \times 20$
\boldsymbol{z}	516	$2 \times 360 2 \times 60$	2×600	
V	544	$2 \times 360 2 \times 60$	2×600	3×150 3×15
\boldsymbol{S}	656	$3 \times 360 3 \times 60$	$1 \times 720 \ 2 \times 600$	
I	700	$3 \times 180 3 \times 30$		

Processing of the Flagstaff data was carried out within the IRAF 1 data reduction software by combining both the aperture and point spread function (PSF) method. Flat-field corrections were obtained from twilight and dome flats. On each of the CCD frames, up to 100 uncrowded stars were selected by multi-aperture photometry to obtain the best fit parameters of the PSF profile. This PSF was then fitted to all detected profiles on each frame. The calibration equations were obtained by observing the standard field of M 67 (Laugalys et al. 2004). For the Flagstaff run 1999 the equations were as follows:

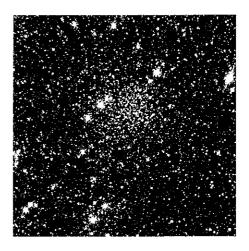


Fig. 1. One of the Flagstaff images of the IC 361 field $(20' \times 20')$ in the *I* filter. North is up, and east is to the left.

$$\begin{split} V &= 1.003\,v - 0.041\,(y-v) - 7.401, \\ U - V &= 1.012\,(u-v) + 0.006\,(y-v) + 0.464, \\ P - V &= 1.033\,(p-v) - 0.178\,(y-v) + 0.474, \\ X - V &= 1.080\,(x-v) - 0.230\,(y-v) + 0.937, \\ Y - V &= 1.073\,(y-v) + 0.413, \\ Z - V &= 1.157\,(z-v) + 1.091, \\ V - S &= 0.916\,(v-s) + 0.550. \end{split}$$

In these equations, the upper-case letters stand for the magnitudes in the standard system, the lower-case letters indicate the instrumental magnitudes corrected for atmospheric extinction. The Flagstaff data of 2009 were transformed to the 1999 system. The zero-points of color indices and the V magnitude in the V indices system were fixed by using five standard stars in the cluster vicinity observed with a photoelectric photometer on the 1.65 m telescope of the Molètai Observatory (Zdanavičius & Zdanavičius 2002). The V-I system is described in Laugalys et al. (2004). The zero point of V-I was fixed using 20 stars selected from the Droege et al. (2006) survey.

The typical single-measurement errors in V magnitude for the two Flagstaff runs and the VATT run are compared in Figure 2. It can be seen that the accuracy of our Flagstaff 1999 photometry is much lower than that of the 2009 run. The errors in VATT photometry obtained in the central part of the cluster do not exceed 0.02 mag down to $V{=}19.0$ mag.

In Figure 3 we show the differences in magnitude V between the two Flagstaff runs (left panel) and the differences in color index U-V between the Flagstaff (average over both runs) and VATT data (right panel). In the final catalog of *Vilnius*

¹IRAF package (http://iraf.noao.edu) is distributed by the National Optical Astronomy Observatory, USA.

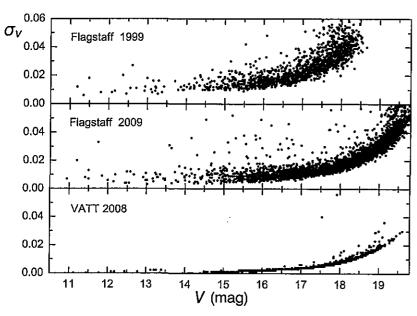


Fig. 2. The single-measurement errors in V from the Flagstaff (two runs) and VATT (central part of the cluster) photometry.

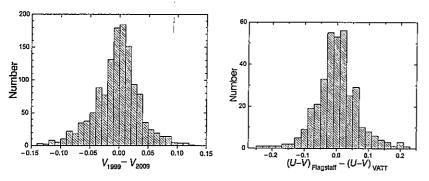


Fig. 3. Differences in magnitude V between the Flagstaff runs of 1999 and 2009 (left panel) and in color index U-V between the Flagstaff (average over both runs) and VATT data (right panel).

photometry (Table 3) the given data are averaged over the three observing runs, Flagstaff 1999, Flagstaff 2009 and VATT 2008, taking into account photometric errors.

To derive the cluster center, a Gaussian function was fit to the distributions of stars on the CCD (in the x- and y-directions) from each exposure in both the V and I filters. The (x,y)-position of the cluster center, acquired in this way, was transformed to the right ascension, declination system using the USNO-B1.0

catalog (Monet et al. 2003) and found to be

$$\alpha = 4^{\rm h}18^{\rm m}55.0^{\rm s}, \, \delta = +58^{\rm o}14'53'' \, (\rm J2000.0).$$

The estimated cluster center is close to the center of our CCD images, but quite different from those given in the WEBDA² database or quoted elsewhere in the literature. The (x,y)-coordinates of stars were transformed to the equatorial system (J2000.0) of the same USNO-B1.0 catalog.

3. CATALOG OF PHOTOMETRY

The catalog of V magnitudes and color indices of 1420 stars down to $V \sim 18.5$ mag both in the standard *Vilnius* system and V-I is given in Table 3, together with the results of photometric classification (see Section 4). Only the stars having X, Y, Z and V magnitudes are included. Therefore, a number of fainter (V>18.5) stars having only U, Y, V photometry from the VATT run are not listed. A colon following the magnitude or color index indicates that the rms error is between 0.05 and 0.10 mag, and a double colon stands for errors of 0.1 mag or larger.

The internal rms errors of the catalog, estimated for five magnitude intervals, are given in Table 2. These were calculated by means of repeated observations as

$$\sigma = \pm \sqrt{\frac{\sum_{N=1}^{N} \sum_{i=1}^{n} (\bar{x} - x_i)}{\sum n - N}},$$

where $(\bar{x}-x_i)$ is the difference between the mean and the individual measurement of each star, n is the number of multiple observations for each star, and N is the number of stars in the catalog in a given magnitude interval.

Table 2. Internal accuracy of the photometric catalog.

V int	erval	N_V	σ_V	σ_{U-V}	σ _P -v	σ_{X-V}	σ_{Y-V}	σ_{Z-V}	σ_{V-S}	σ_{V-I}
10.00	15.00	91	0.009	0.024	0.021	0.022	0.012	0.013	0.012	0.016
15.00	16.50	350	0.011	0.036	0.030	0.025	0.014	0.016	0.014	0.020
16.50	17.50	468	0.017	0.050	0.045	0.033	0.023	0.021	0.020	0.029
17.50	18.00	324	0.027	0.043	0.071	0.047	0.038	0.030	0.032	0.039
18.00	18.50	201	0.030	0.032	0.094	0.057	0.045	0.035	0.038	0.046

A complete catalog of Flagstaff V,I photometry, which contains 7250 stars down to I=19.6 mag in the $20'\times 20'$ field, and the catalog of VATT U,Y,V photometry with 806 stars down to V=19.6 mag in the central part of the cluster field $(12'\times 12')$, are available in electronic form and can be supplied by the authors on request.

The color-magnitude diagrams for stars common to the VATT U, Y, V and Flagstaff V, I data sets are shown in Figure 4.

4. QUANTITATIVE CLASSIFICATION OF STARS

For the determination of spectral classes, absolute magnitudes M_V and values of interstellar extinction $(A_V = RE_{Y-V})$ of individual stars (we call this process a quantitative classification) we used a few different codes.

²http://www.univie.ac.at/webda/

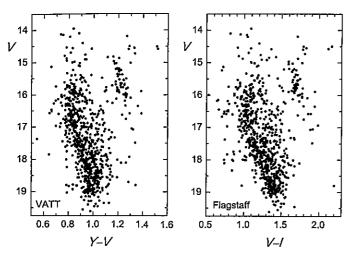


Fig. 4. The V vs. Y-V diagram with the VATT data (left panel) and the V vs. V-I diagram with the Flagstaff data (right panel). The number of stars in each panel – 782.

(1) COMPAR code, based on the so-called σQ -method (Straižys et al. 2001a). The principle of the method is matching 14 different interstellar reddening-free Q-parameters of a program star to those of about 8400 standard stars of various spectral and luminosity classes, metallicities and peculiarity types. This code selects a number of standard stars which have a set of Q-parameters most similar to those of a program star. If the σQ values are sufficiently small (i.e. Q-differences between a program star and the closest standard stars are small), the average parameters of the closest standard stars will be assigned to that program star. σQ is a function of the accuracy of photometry, the uncertainty in stellar parameters of standard stars and the degree of representation of various types of standard stars included. For photometry of Population I stars with the 1% accuracy, σQ is usually of the order of $\pm (0.01-0.02)$ mag.

(2) xqKLAS code, based on the so-called xq-method developed by Zdanavičius (2005). The method relies upon a new concept of reddening-free parameters (q) and a 'virtual' quantity of the interstellar dust (x). 1418 standards are formed by calculating the mean dereddened color indices for 89 spectral subclasses (mostly for each one subclass or, in the case of late-type stars, for each 0.25 subclass) and 17 values of the absolute magnitude M_V . The code takes into account the errors of photometry and, as a final result, gives for each program star its spectral type, M_V , interstellar extinction A_V and distance from the sun.

(3) TINKLAS code, which classifies stars using six Q,Q diagrams as described in Straižys (1992). Each of such diagrams is formed from two reddening-free Q-parameters and calibrated in terms of spectral classes and absolute magnitudes.

(4) dxq method, developed recently by one of the authors (K. Z.), uses a combination of ten $\dot{V}ilnius$ color indices of 300 standards of solar chemical composition. These standards represent a variety of spectral and luminosity classes with known mean intrinsic color indices. As a first step, the color indices of each observed star are compared with those of standards to find the differences for each of the ten

color indices. Then, using these differences and the color excesses for unit mass of interstellar dust, derived from the interstellar extinction law, the values of dust mass are calculated for each color index of each standard. Finally, the parameters of the standard which gives the least scatter in dust mass calculated using the ten color indices are ascribed to the star under classification.

Spectral classes and absolute magnitudes of program stars determined by methods (2), (3) and (4) were used to estimate luminosity classes according to MK type calibrations in M_V from Straižys (1992). The intrinsic color indices $(Y - V)_0$ used for the determination of E_{Y-V} were also taken from Straižys (1992). The values of A_V were calculated with $R = A_V/E_{Y-V} = 4.16$ for the normal interstellar extinction law (Straižys et al. 2001b).

It should be noted that the above four codes use slightly different sets of spectral standards. However, the comparison of the classifications shows that the four methods give results generally in good agreement. For a total of 1225 stars, the average difference between the spectral classes derived by dxq and COMPAR codes was found to be 1.8 subclasses. For stars of spectral type F5 and later types (268 stars), this difference is only 1.2 subclass. Spectral types of about 50 stars, mainly of early types, differ more than by 5 spectral subclasses. The difference of dereddened and intrinsic color indices calculated by the dxq method is shown in Figure 5.

The results of quantitative classification, i.e. spectral types, the values of interstellar extinction A_V and distances are given in Table 3, together with the catalog of observations. Poor quality classification data (the difference between 0.05 and 0.10 mag) are marked by a colon, and those with larger uncertainties (0.1 mag or larger) are indicated with a double colon. For about 250 stars in the table, mainly of A-G types at fainter magnitudes, no luminosity classes were determined. For these, the intrinsic color indices of luminosity class V were ascribed when calculating the values of interstellar extinction. Since the cluster stars are slightly metal-deficient (Zdanavičus et al. 2009a), the classification using standards of only solar abundances may lead to a slight overestimate of distances.

5. DISCUSSION AND CONCLUSIONS

In Figure 6 (left panel) we show the distribution of individual distance moduli $(m-M)_0$ for the sample of 1225 stars. If we assume that the second peak of the distribution at $(m-M)_0=12.8$ mag (as well as the concentration of points in the right-panel diagram) represents the cluster population, we may suggest that IC 361 is located as far as, or just beyond, the Perseus arm. The first peak seen at slightly smaller distance is probably due to unresolved binary stars.

The dependence of interstellar extinction on the distance moduli is demonstrated in the A_V vs. $(m-M)_0$ diagram (right panel of Figure 6). The two principal features to note in this figure are (1) the heavy concentration of points in the vertically elongated area centered approximately at $(m-M)_0=12.8$ and $A_V=2.2$ mag, which can be considered to be the concentration of the cluster members, and (2) the spread of A_V values at this particular distance. It is evident from the scatter that interstellar extinction A_V is non-uniform across the cluster field, with the values of A_V ranging from 1.9 to 2.4 mag.

The evidence for variable extinction also comes from IRAS 100 μ m thermal

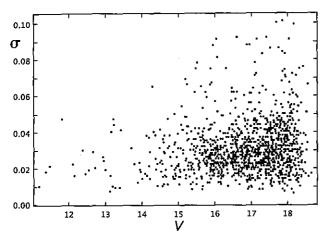


Fig. 5. The mean differences between the dereddened and standard intrinsic color indices of 1225 stars classified by the xdq method.

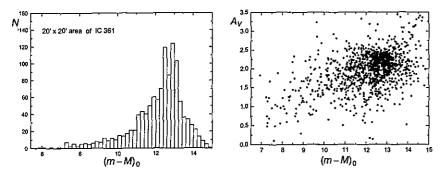


Fig. 6. Distribution of true distance moduli (left panel) and the A_V vs. distance modulus diagram (right panel).

emission image taken from SkyView Virtual Observatory³, which is shown in Figure 7. According to the reddening calibrations of dust maps by Schlegel et al. (1998), the values of E_{B-V} across IC 361 are in the range 0.79 to 0.90 mag, with corresponding A_V values from 2.4 to 2.8 mag.

A non-uniform extinction across the cluster complicates fitting the color magnitude diagram to theoretical isochrones and, consequently, the determination of age and other basic parameters. In such a case, the use of photometric parameters of individual stars becomes a crucial point. The results of seven-color photometry and quantitative classification of individual stars obtained in the present paper (Table 3) will be used in the forthcoming paper on the fundamental parameters of IC 361.

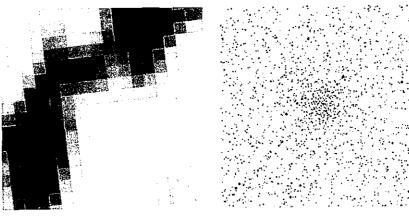


Fig. 7. Left panel: the IRAS 100 μm map of the field around IC 361. Right panel: the cluster image in DSS2 Red. Both maps have the same center and the same size, $25' \times 25'$.

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³http://skyview.gsfc.nasa.gov/

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Table 3. Results of photometry, photometric classification, interstellar extinctions and distances for stars in the IC 361 area.

tinc	tions and	dist	an	ces	ior s	tars I	n tne	IC a	от а 	rea.					
No	RA(2000)	DEC	3(20	000)	\overline{v}	U-V	P-V	<i>X-V</i>		Z- V	V-S	V-I	Photom.	A_V	đ
2.0.	hm s	0		11		mag	mag	mag	mag	mag	mag	mag	sp. type	mag	рс
						 -							10011	0.61	
1	4 17 42.3				16.05		3.33						k3.2 V: a1.5 V:	0.61 2.52	560
2	4 17 42.4	+58	17	24	15.74	3.08	2.71	1.67:	0.04	0.40	0.60	1 19	g1.5 IV	0.02	1970
3	4 17 42.4	+58	20	J3	17.55	3.19	2.00	1.00	0.00	0.31	0.03	0.04	a1.5 V-III	2.58	5050
4	4 17 46.7 4 17 46.8	+58 +58			18.11		2.12:		0.92:				a1.0 V-111	2,00	0000
5 6	4 17 40.8	+58			18.09				1.02:						
7	4 17 47.8	+58				3.53	2.65						a8 V	2.16	1160
8	4 17 48.6	+58			16.46		2.69		0.81	0.33	0.65	1.10	a4 V	2.33	
9	4 17 48.8	+58			17.35			1.85	0.95	0.34	0.84	1.37			
10	4 17 48.9	+58			16.74		2.68						g1 IV		3410
11	4 17 49 1	+58				4.81:	3.99						g9.5 III	1.85	4100
12	4 17 49.2	+58			17.77			1.63		0.42			211		1000
13	4 17 49 2	+58			16.95			1.57					a2 V:	2.34	
14	4 17 49.5	+58			17.73								g5.5 V	1.49	1710
15	4 17 49.6	+58			17.52	3.44	2.84	1.93		$0.40 \\ 0.36$					
16 17	4 17 50.1 4 17 50.3	+58 +58				3.44	9 44		0.53	0.30	0.72	0.02	111 00	2.06	4780
18	4 17 50.3	+58			17.78	0.44	2.44	1.88	0.13	0.20	0.55	1 21	a2 III g1 IV		5580
19	4 17 51.0	+58			17.80				1.08:				6		0000
20	4 17 51.5	+58			15.98	3.72	3.07	2.16					g4 IV	1.57	1950
21	4 17 52.2	+58				3.72							g8 IV	1.09	1160
. 22	4 17 52.3	+58			16.88			2.62			0.99			4.20	
23	4 17 52.7	+58			17.54				1.02				g6 IV		3780
24	4 17 52.9	+58	16	10	17.96				0.89	0.36	0.79	1.24	g4 V		2390
25	4 17 53.3	+58				3.45	2.72		0.94	0.34	0.78	1.27	f7 IV		1910
26	4 17 53.4	+58			17.98				1.12:				f2 V-III	2.80	2730
27	4 17 53.7	+58			17.63		3.25::			0.43			61.7.6	1.05	1500
28	4 17 54.1	+58			15.61	3.28	2.61	1.78	$0.89 \\ 0.91$				f1 V: a1 V:	2.73	1520
29	4 17 54.1	$+58 \\ +58$			18.25 15.77	4 En.	9 70	2.72					g9 IV		1240
30 31	4 17 54.8 4 17 55.2	+58			14.98			1.53		0.26	0.63	0.94	a4 V	1.97	
32	4 17 55.2	+58			18.15	0.05	Dioo						g5.5 V		1950
33	4 17 55.6	+58			16.53	3.73:	2.68	1.67					a3 V-III	2.43	
34	4 17 56.0	+58					2.82		0.98	0.37	0.87	1.37	f7 III	1.86	4170
35	4 17 56.1	+58		14	15.06	4.52	3.77	2.62	1.16	0.43	1.02	1.62	g9.5 III	1.44	3790
36	4 17 56.2	+58	25	20	17.87:	!			0.95:						
37	4 17 56.7	+58		09	18.27				0.97:				a0.5	3.39	
38	4 17 56.8	+58			17.73				1.51		1.63				
39	4 17 56.9	+58			17.00			2.77	1.09				k3.7 V	1.42	570
40	4 17 57 0	+58			17.00		2.69:	1.90	1.00:	0.31	0.87		f0 V-IV	2 .52	9400
41	4 17 57.2	+58			17.11		2.60		0.83					1.71	2400
42 43	4 17 57.6 4 17 57.6	+58 +58			17.51	3.93:	2.83						a3 IV:		4190
44	4 17 57.6				17.33	3.95.							a5 V-III	2.29	
45	4 17 57.8	+58		06	15.20	5.03:			1.25				k0 III:		3250
46	4 17 57.9	+58		09	17.55			2.17:	1.02:				g0 V-IV		1780
47	4 17 57.9	+58				3.68:		1.67	0.82	0.34	0.69	1.09	a1.5 V	2.57	
48	4 17 58.1	+58	21	55			2.81:						a0 V-III	3.09	
49	4 17 58.2	+58		01	17.94				1.07:						5020
50	4 17 58.4	+58				3.38:								2.04	
51	4 17 58.8	+58				4.68:	3.90						g8 III	2.05	
52	4 17 59.0	+58			17.42	0.00	0.00		1.29				g8 IV	2.55	
53	4 17 59.1				15.62	3.29	2.09	1.81					f6 IV a6 V	1.61 2.36	
54	4 17 59.2	+58			17.73		4.10						ao v g1.5 V	1.46	
55 56	4 17 59.2 4 17 59.5	+58			17.36		2 70.	2.01	0.92:	0.30	0.00	1.49	69.5 V		1860
56 57	4 17 59.5				18.08		2.10:	2.08	0.95	0.36	0.851	1.39	f9.5 V g4 V-III	1.49	
58	4 17 39.9	+58			16.99			2.42	1.10	0.44	1.02	1.58	g4 V-III g8 V k0 III	1.97	
59	4 18 00.0	+58			15.88		4.21	2.97	1.31	0.50	1.17	1.91	k0 III	2.13	
60	4 18 00.1				18.00			2.05:	0.99	0.32	0.94	1.42			
61	4 18 00.5				17.66		2.75:	1.73:	0.85	0.34	0.71	1.16:	a1.5 V	2.71	5880
		, -													

Table 3. Continued

Ta	ipie a. C	OHU	mue	ea											
No.	RA(2000)	DEC	(20	00)	\overline{v}	U~V	P– V	X-V	$Y \neg V$	ZV	V– S	V-I	Photom.	A_V	d
	hm s	0			mag	mag	mag	mag	mag	mag	mag	mag	sp. type	mag	рс
62	4 18 00.6	+58	07	56	16.59		2.61:	1 81	0.87	0.31	0.80	1.22	f1 V-III	2.03	2190
63	4 18 00.7	+58			15.97		3.89		1.26				g6 III		3590
64	4 18 01.1	+58	09	25	17.76		2.62:			0.31					
65	4 18 01.2	+58			17.70		2.66:	1.72:	0.83:	0.23	0.77:	1.17	a7 V-III	2.24	4490
66	4 18 01.2	+58	16	22	15.52	4.22			0.99	0.47	0.93	1.42	k0.7 IV	0.95	
67	4 18 01.2	4.58	13	28	17.85			1.88		0.33					
68	4 18 01.3	+58	18	45	18.44			2.22:		0.42					
69	4 18 01.4	+58	22	50	17.08			2.90	1.19					1.90	
70	4 18 01.7	+58	07	32	16.86		2.74:	2.01	0.96				f9.5 V	1.73	
71	4 18 01.8						0.70.	2.88	1.10	0.04	0.05	1.00	k4.5 V f3 IV	1.27 2.22	
72 73	4 18 02.1 4 18 02.2				17.44 17.34		2.79: 2.76	1.99	0.97				60 V-IV	2.34	
74	4 18 02.2	+58			17.68		2.70	2.93:					k5.5 V	1.12	
75	4 18 02.6					3.43	2.64		0.89		0.78			2.03	
76	4 18 02.7	4.58	23	34	17.85		2.76.	1.87:	0.93:	0.28:	0.81:	1.19:	a9 V-III	2.38	
77	4 18 02.7	+58	08	08	17.23		2.57:	1.80	0.87	0.31	0.83	1.24	f2 V	1.94	
78	4 18 02.8	+58	22	54	15.25	5.33:	4.40	3.15	1.35	0.52	1.20	1.95		2.30	2820
79	4 18 02.8	+58	18	37	18.14		2.87::	1.99	0.97	0.41	Ų. 9	1.27	IU	2.49	
80	4 18 02.9				17.75				0.82	0.35	0.89	1.36	g9.5 V	0.90	
81	4 18 03.3			03	15.32	3.01	2.19	1.25						1.73	
82	4 18 03.6			56	16.63	3.33	3.86:	2.87					g4 III f9.5 IV	$\frac{2.69}{1.44}$	1500
83		+58		42	16.59	3.33	2.69	2.69		$0.34 \\ 0.49$	1 02	1.20	g9 IV	2.06	10//0
84 85	4 18 04.2	+58 +58			17.67			2.27:					goiv	2.00	1340
86	4 18 04.4	+58				5.14:							k0.5 III	1.99	2780
87	4 18 04.4	+58			18.30		7.20	2.00:		0.37				1.69	
88	4 18 04.5	+58				4.46	3.73						k0.7 IV:		1610
89	4 18 04.5	⊹58		11	13.93	3.61	3.04	2.08	0.88	0.36	0.82	1.17	g9.5 IV	0.65	
90	4 18 04.6	+58	10	18	18.15								f2 V-III	2.40	3550
91	4 18 04.6	+58	14	54	17.59		2.72:	1.76	0.86	0.33	0.75	1.17			
92	4 18 05.0	+58	21	10	17.85	3.31::	2.63:	1.75	0.89:	0.31	0.73	1.17	f2 III::	1.66	
93					18.03								m0 V		399
94		+58				3.75:		2.00						2.36 1.67	
95 96					16.71	3.70	$\frac{2.64}{2.93}$							1.96	
97		+58		27	15.40	4.64:	3.78	2.70		0.45				1.50	2020
98	4 18 06.3	+58		11	16.54:	3.82:	2.99	2.13					f3 IV	2.53	2130
99	4 18 06.5	+58			15.99			3.05					k5.5 V	1.23	296
100	4 18 06.7				17.89			2.72:					g3 IV	2.87	2620
101	4 18 06.8	+58	16	14	17.68		2.63:	1.61	0.75	0.31	0.54	0.89	a4 V:	2.07	6360
102	4 18 06.9	+58	14	80	16.99	3.66: 3.35	2.65	1.70	0.79	0.28	0.67	1.05	a8 III	1.97	6000
103		+58	17	03	15.93	3.35	2.63	1.86	0.92	0.35	0.78	1.22	f6 IV	1.69	2160
104					17.64		2.64:	1.80	0.84:	0.38	0.71	1.12			
105	4 18 07.3	+58			17.05	3.60:	0.65							2.65	5500
106 107		+58 +58		22	16.09	3.00:	2.61	1.01:	0.60:	0.25.	0.01.	1.16	f6 IV	1.64	2370
108		+58		14	16.88	3.61	2.75	1.88	0.92	0.34	0.81	1.32		2.32	
109	4 18 08.3	+58		02	16.02	4.30	3.60	2.51	1.12	0.43	1.02	1.59	g9.5 IV	1.68	
110	4 18 08.4				17.99		2.69::		0.90:	0.31	0.85:	1.17		2.28	
111	4 18 08.5	+58	27	08	14.20	3.02	2.38	1.64	0.77	0.34	0.60	0.95	f6 IV	1.14	1250
112	4 18 08.5				17.63			1.77	0.86	0,33	0.63	1.10			
113	4 18 08.6	+58	22	47	17.32	3.65:	2.64	1.83	0.91	0.31	0.77	1.15			
114		+58	23	04	18.05		2.47:	1.79:	0.75:	0.27:	0.86:	1.21	g1 V a3 V-III f9 V-III	1.03	3250
115	4 18 08.8	+58	08	15	17.06		2.55:	1.52	0.75	0.23	0.61	1.03	a3 V-III		5110
116	4 18 08.9	+58	12	47	18.07	0 10		1.94:	0.93	0.33	0.87	1.31	19 V-III		2870
117	4 18 08.9	+58	24	29	14.93	3.48	2.68	1.80	0.92	0.33	0.77	1.23		1.98	1000
118					16.91		0.00	2.53					g4 III	1.96	2170
119					17.22				0.99:	U.44;	0.70	1.20	f6 V: g4 V-III	1.54	
120	4 18 09.4 4 18 09.6	+58 +58			17.49	3.34:	2.89:	1 76		0.41			P4 A-TIT	1.04	1040
121 122	4 18 09.6	+58				3.34: 4.41:							k1.5 V	1.88	360
123		+58			16.78		2.62	1.86					f9 IV	1.34	
124						3.33:							fi V:	1.95	
125	4 18 10.3	+58	14	40	17.33	3.58	2.69	1.84	0.92	0.35	0.77	1.26	f0 V	2.24	3010
									-			_			

Table 3. Continued

No. Na Na Na Na Na Na Na N	S.L	thie o. C	Ontinued											
1.52 2.880 1.52 1.52 1.53 1.52 2.890 1.25 0.55 1.05 1.70 1.51 1.52 2.890 1.22 4.18 10.5 +5.86 10.7 1.50 1.50 2.800 1.52 0.55 0.05 0.	No.	RA(2000)	DEC(2000)	V U	<i>t-v</i> .	P– V	X– V	Y-V	Z– V	V– S	V-I	Photom.	A_V	d
1.59		hm s	0 / //	mag m	iag 1	mag	mag	mag	mag	mag	mag	sp. type	mag	рc
1.59			1 50 00 51	14 47 5	OF .	4 05	2.06	1 25	0.55	7.05	1 70	k1 5 III	1.52	2890
1.86 1.86 1.85 1.86 1.67 1.86 1.86 1.86 1.31 1.85 1.25 1.50 1.32 2870						4.20								
120									0.31	0.82	1.25:	g0 V		
130 4 18 1.1					.56	2.66		0.94	0.36	0.82	1.29	f4 IV		
131 4 18 1.1.1 +58 11 68 17.55 132 4 18 1.1.4 +58 06 57 18.03 133 4 18 1.1.4 +58 06 57 18.03 134 4 18 1.1.4 +58 06 57 18.03 134 4 18 1.1.4 +58 06 57 18.03 135 4 18 1.1.4 +58 06 57 18.03 136 4 18 1.1.4 +58 06 57 18.03 136 4 18 1.1.4 +58 07 17.05 138 4 18 1.2.2 +58 23 47 16.98 139 4 18 1.2.7 +58 21 09 17.95 4.28 140 4 18 1.3.0 +58 22 42 15.22 3.64 141 4 18 1.3.0 +58 22 42 15.22 3.64 142 4 18 1.3.2 +58 23 13.14 2.99 143 4 18 1.3.4 +58 19 43 15.33 3.65 145 4 4 18 1.3.4 +58 13 13 146 4 4 18 1.3.4 +58 13 18 147 4 18 1.3.5 +58 27 23 17.33 3.63 148 4 4 18 1.3.6 +58 26 59 17.09 3.65 150 4 4 18 1.3.6 +58 26 59 17.09 3.55 151 4 4 18 1.3.4 +58 15 31 152 4 4 18 1.3.5 +58 60 17 19 153 4 18 1.4 +58 15 17 17 155 4 18 1.4 +58 15 17 17 156 4 4 18 1.3.6 +58 26 50 17.09 3.65 150 4 4 18 1.3.6 +58 26 50 17.09 3.65 152 4 4 18 1.3.5 +58 60 17 19 3.65 154 4 4 1.5 4 50 17 19 3.65 155 4 4 18 1.3.6 +58 26 50 17.09 3.65 156 4 4 18 1.5 +58 00 17.90 3.65 156 4 4 18 1.5 +58 00 17.90 3.66 156 4 4 18 1.5 +58 00 17.90 3.66 157 4 4 18 1.5 +58 00 17.80 158 4 4 18 1.5 +58 00 17.90 3.66 157 4 4 18 1.5 +58 00 00 00 00 00 00 00													0.69	-
132 4 18 11.4 58 66 57 18.03 34 18 11.4 58 66 57 18.03 34 18 11.8 58 27 08 18.00 35 4 18 11.9 58 19 40 15.38 3.66 36 4 18 12.1 58 67 47 17.13 37 4 18 12.1 58 23 47 16.98 38 4 18 12.2 58 23 47 16.98 38 4 18 12.6 58 16 34 16.18 4.48 3139 4 18 13.0 58 27 17 18.35 414 4 18 13.0 58 27 17 18.35 414 4 18 13.0 58 27 17 18.35 414 4 18 13.0 58 27 17 18.35 414 4 18 13.2 58 17 33 17.13 4.20 42 4 18 13.4 58 19 31 33 3.56 44 4 18 13.4 58 63 03 17.13 44 4 18 13.4 58 63 03 17.13 44 4 18 13.5 58 17 23 17.35 3.63 46 4 4 18 13.5 58 17 23 17.35 3.63 47 4 4 18 13.6 58 26 59 17.09 3.53 418 4 4 4 4 4 58 3 5 4 4 4 4 58 3.5 58 65 67 68 68 4 4 4 4 58 67 67 68 50 4 4 4 58 67 67 68 50 4 4 4 58 67 67 68 50 4 4 4 58 67 67 68 50 4 4 4 58 57 67 68 50 4 4 4 58 57 67 50 4 4 4 58 57 57 18 50 4 4 4 58 57 67 50 4 4 4 58 67 67 50 4 4 4 58 67 67 50 4 4 4 58 57 67 50 4 4 4 58 57 67 50 4 4 4 58 57 67 50 4 4 4 58 57 67 50 4 4 4 58 57 67 50 4 4 4 58 67 67 50 4 4 67 67 67 50 4 4 67 67 67 50 4 4 67 67 67 50 4 67 67 67 67 67 50 4 67 67 67 67 67 50 4 67 67 67 67 67 67 67													2.45	2630
133 4 18 11.4 58 05 18 17.85 134 4 18 11.8 58 27 08 18.00 135 4 18 11.9 58 19 40 15.38 3.66 136 4 18 12.1 58 07 47 17.13 137 4 18 12.2 58 23 47 16.98 138 4 18 12.7 58 21 09 17.95 4.28 140 4 18 13.0 58 22 17 18.35 141 4 18 13.0 58 22 15.22 3.64 142 4 18 13.2 58 22 13 13 2.99 144 4 18 13.2 58 22 13 13 2.99 144 4 18 13.4 58 19 43 15.33 3.66 145 4 4 18 13.4 58 19 43 15.33 3.66 146 4 4 18 13.4 58 19 43 15.33 3.66 147 4 4 18 13.4 58 19 43 15.33 3.66 148 4 4 18 13.4 58 19 43 15.33 3.66 149 4 4 18 13.4 58 19 43 15.33 3.66 140 4 4 18 13.4 58 19 43 15.33 3.66 140 4 4 18 13.4 58 19 43 15.33 3.66 140 4 4 18 13.4 58 19 59 17.09 3.66 140 4 4 18 13.5 58 65 17.09 3.66 140 4 4 18 13.6 58 26 59 17.09 3.66 140 4 4 18 13.6 58 26 59 17.09 3.66 140 4 4 18 13.6 58 26 59 17.09 3.66 140 4 4 4 58 77 30 30 140 4 4 4 4 58 77 30 30 140 4 4 4 4 58 77 30 30 140 4 4 4 4 58 77 30 30 140 4 4 4 4 58 77 30 30 140 4 4 4 4 58 77 30 30 140 4 4 4 4 58 70 30 30 140 4 4 4 4 58 70 30 30 140 4 4 4 4 58 70 30 30 140 4 4 4 4 4 4 4 4 4														
134 4 18 11.9 +58 19 40 15.38 3.66 2.49 1.82 2.09 1.96 0.37 0.87 1.30 1.51 1.64 1480 1.35 1.64 1480 1.35 1.64 1480 1.35 1.64 1480 1.35 1.3													3.36	5350
135 4 18 11.9 +58 19 40 15.38 3.66 2.95 2.08 0.96 0.37 0.87 1.30 g1.51V 1.66 1396 320 321								0.94:	0.35:	0.71:	1.11:			
138 4 18 12.6 +58 15 34 16 18 44 48 3.75 2.99 1.30 0.47 1.22 1.93 g.5 11 1.05 1.62 g9V 2.14 1050 1.30 4 18 13.0 +58 27 17 18.35 2.56 1.17 0.51 1.05 1.62 g9V 2.14 1050 1.44 18 13.0 +58 27 27 18.35 2.68 2.02 0.97 0.32 0.94 1.43 g0 V 1.56 3120 1.44 18 13.4 +58 12 31 13.4 2.99 2.39 1.86 0.75 0.28 0.69 0.96 19 V 1.56 3120 1.44 18 13.4 +58 13 51 6.00 4.60 3.69 2.63 1.21 0.47 1.11 1.74 g.5 III 1.75 1.36 1.44 1.81 1.84 +58 1.75 1.56 0.60 6.60 0.76 0.29 0.67 1.03 41 V 1.56 3120 1.44 1.81 1.84 +58 1.75 1.56 0.60 6.60 0.76 0.29 0.67 1.03 41 V 1.56 3120 1.44 1.81 1.84 +58 1.75 1.35 0.28 0.89 0.80 0.96 1.75 0.91 0								0.96	0.37	0.87	1.30	g1.5 IV	1.64	1480
138 4 18 12.6 +58 15 34 16 18 44 48 3.75 2.99 1.30 0.47 1.22 1.93 g.5 11 1.05 1.62 g9V 2.14 1050 1.30 4 18 13.0 +58 27 17 18.35 2.56 1.17 0.51 1.05 1.62 g9V 2.14 1050 1.44 18 13.0 +58 27 27 18.35 2.68 2.02 0.97 0.32 0.94 1.43 g0 V 1.56 3120 1.44 18 13.4 +58 12 31 13.4 2.99 2.39 1.86 0.75 0.28 0.69 0.96 19 V 1.56 3120 1.44 18 13.4 +58 13 51 6.00 4.60 3.69 2.63 1.21 0.47 1.11 1.74 g.5 III 1.75 1.36 1.44 1.81 1.84 +58 1.75 1.56 0.60 6.60 0.76 0.29 0.67 1.03 41 V 1.56 3120 1.44 1.81 1.84 +58 1.75 1.56 0.60 6.60 0.76 0.29 0.67 1.03 41 V 1.56 3120 1.44 1.81 1.84 +58 1.75 1.35 0.28 0.89 0.80 0.96 1.75 0.91 0								0.78	0.27	0.65	1.01	a7 V-III	1.96	3920
138 4 18 12.6 5-58 16 34 16.18 4.48 3.75 2.66 1.12 0.44 1.05 1.62 g9f 1.20 4.452 1.40 1.41 1.11 1.			+58 23 47	16.98			2.99	1.30	0.47	1.22	1.93	g8.5 III		
18		4 18 12.6		16.18 4.	.48									
141	139	4 18 12.7		17.95 4.	.28								2.14	1050
143 4 18 13.4 +58 19 43 15.33 3.56	140	4 18 13.0	+58 27 17						0.34:	0.88:	1.29:			
143 4 18 13.4 +58 19 43 15.33 3.56	141	4 18 13.0							0.32	0.94	1.43	gUIV		
143 4 18 13.4 +58 19 43 15.33 3.56	142	4 18 13.2							0.46	0.98	1.51	g91V		
146	143								0.28	0.69	0.96	INIA		
146	144				.56	2.62				0.67	1.03	841V		
147 4 18 13.4 +58 12 17.3 17.3 3.63 2.69 1.72 0.83 0.30 0.78 1.21 a.71V 2.22 5170 148 4 18 13.6 +58 26 59 17.09 3.55 2.64 1.77 0.86 0.42 0.62 1.06 a.9V 2.09 3010 150 4 18 13.6 +58 24 56 15.28 4.61 3.80 2.68 1.22 0.46 1.03 1.62 151 4 18 13.8 +58 15 67 17.01 3.50 2.64 1.81 0.88 0.32 0.78 1.24 10V 2.14 2720 152 4 18 13.9 +58 18 54 18.22 3.57 2.64 1.81 0.88 0.32 0.78 1.24 10V 2.14 2720 153 4 18 14.1 +58 15 01 17.90 3.86 2.88 2.03 0.94 0.32 0.78 1.24 10V 2.14 2720 155 4 18 14.1 +58 15 01 17.90 3.86 1.75 0.89 0.34 0.74 1.21 a.55 0.96 6750 155 4 18 14.4 +58 17 51 18.23 3.62 1.56 0.83 0.94 0.32 0.91 1.39 g5V-IV 1.78 2400 157 4 18 14.4 +58 17 51 18.23 3.62 1.56 0.83 0.88 1.32 0.91 1.39 g5V-IV 1.78 2.40 0.84 1.75 1.85 0.96 0.30 0.95 1.44 1.24 0.58 0.95 0.95 0.30 0.95 1.44 1.24 0.58 0.95 0.95 0.95 0.30 0.95 1.44 1.24 0.58 0.95 0														
148 4 18 13.5 +58 17 23 17.35 3.51 2.66 1.65 0.78 0.29 0.67 1.06 a5 V 2.13 4840 149 4 18 13.6 +58 26 59 17.09 3.53 2.64 1.77 0.86 0.42 0.62 1.03 a9 V 209 301 301 301 302 303 303 303 303 303 151 4 18 13.8 +58 16 57 17.01 3.50 2.64 1.81 0.88 0.32 0.78 1.24 10V 2.14 2702 152 4 18 13.9 +58 18 54 18.22 3.57 2.18 1.00 0.39 0.92 1.38 3.54 5.15 0.15 3.41 1.45 1.05 3.66 3														
149														
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18								0.80	0.42	1.02	1.00	as v:	2.09	3010
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154						2 88.		0.04	0.32	0.91	1.39	95 V-III		
185 4 18 14.2 +58 22 40 14.89 4.61 3.58 2.66 1.26 0.43 1.13 1.85 f7 III 3.23 850 156 4 18 14.4 +58 27 48 13.21 6.61 5.56 3.96 1.56 0.78 1.34 2.31 15 III 1.96 1620 157 4 18 14.4 +58 17 51 18.23 3.62 1.85 0.96 0.30 0.95 1.44 f2 V - III 2.28 3860 160 4 18 14.8 +58 0.59 16.88 2.53 1.69 0.83 0.28 0.73 1.18 a9 V - III 1.99 2870 1.62 4 18 15.3 +58 0.61 17.78 1.55 0.75 0.25 0.60 1.01 a3 V - III 1.99 2870 1.62 4 18 15.5 +58 0.61 17.78 1.55 0.75 0.25 0.60 1.01 a3 V - III 1.93 2870 1.64 4 18 15.6 +58 0.33 15.70 2.77 2.05 1.27 0.64 0.23 0.57 0.80 a9 V 1.06 2560 1.64 4 18 15.9 +58 13 6 18.04 4.09 2.43 1.08 0.45 0.99 1.39 20 V 1.63 2.55 0.96 0.30 0.95 1.44 4 4 4 4 4 4 4 4 4						2.00.			0.34	0.74	1.21	a0.5 V		
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159									0.30	0.95	1.44	f2 V-III:	2.28	3860
160					.14	3.25	2.09	1.05	0.44	1.13	2.05	a7 IV:	3.18	2730
181 14 18 14 9 +58 10 15 18 18 12 3.66 17.78 1.55 0.75 0.25 0.60 0.10 3 \ V-III 1.83 2150 1.63 4 18 15.5 +58 0.61 2 18.25 1.93 0.88 0.33 0.90 1.39 0.90 1.39 0.90 1.55 3010 3 \ V-III 1.55 3010								0.83	0.28	0.73	1.18	a9 V-III	1.99	2870
162 4 18 15.3 +58 06 16 17.78 1.55 0.75 0.25 0.60 1.01 a3V-III 2.11 7130 1.64 4 18 15.6 +58 08 31 15.70 2.77 2.05 1.27 0.64 0.23 0.57 0.80 a9V 1.06 2560 1.65 4 18 15.9 +58 17 4 18 16.1 +58 12 30 16.88 3.72 2.72 1.70 0.81 0.28 0.70 1.11 a4V-III 2.37 3820 1.68 4 18 16.1 +58 12 30 16.88 3.72 2.72 1.70 0.81 0.28 0.70 1.11 a4V-III 2.37 3820 1.68 4 18 16.2 +58 05 28 16.71 2.65 1.87 0.89 0.30 0.79 1.25 12 1.70 2.30 1.70 4 18 16.5 +58 05 28 16.71 2.65 1.87 0.89 0.30 0.79 1.25 12 1.90 3.06 1.01 1.30 1.01 1.30 1.01 1.30 1.01 1.0				18.22 3	.66		2.26:	1.00						
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180 4 18 17.5 +58 10 58 17.50 3.64 2.70: 1.98 0.99 0.34 0.89 1.38 183 181 4 18 17.5 +58 20 23 17.60 3.58 2.62 1.65 0.74 0.28 0.63 0.95 a5 V-III 2.09 5520 182 4 18 17.6 +58 21 49 17.00 3.58 2.80 1.96 0.93 0.38 0.81 1.30 f3 IV 2.12 3190 183 4 18 17.6 +58 16 05 17.79 3.71 2.67: 1.77 0.88 0.29 0.81 1.25 184 4 18 17.6 +58 16 18 17.79 3.71 2.67: 1.78 0.88 0.31 0.77 1.22 10 III 2.04 7410 185 4 18 17.6 +58 17.20 3.00: 2.17 1.00: 0.42 0.83 1.26 g1 IV 1.79 325						2.75		0.97	0.37	0.85	1.31	f4 IV		
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182 4 18 17.6 +58 21 49 17.00 3.58 2.80 1.96 0.93 0.38 0.81 1.30 f3 IV 2.12 3190 183 4 18 17.6 +58 16 92 16.22 3.89 2.70 1.77 0.88 0.29 0.81 1.25 184 4 18 17.6 +58 16 57 3.71 2.67 1.78 0.88 0.31 0.77 1.22 f0 III 2.04 7410 185 4 18 17.6 +58 25 50 17.20 3.00 2.17 1.00 0.42 0.83 1.26 g1 IV 1.79 3250 187 4 18 17.7 +58 19 32 16.08 4.97 4.13 2.92 1.26 0.49 1.15 1.83 k0 III 2.00 4740 188 4 18 17.7 +58 23 19 14.63 3.30 2.52 1.63 0.77 0.27 0.69 0.97 a9 V 1.83 1100												a5 V-III	2.09	5520
183 4 18 17.6 +58 09 29 16.22 3.89 2.70 1.77 0.88 0.29 0.81 1.25 184 4 18 17.6 +58 16 05 17.79 3.71 2.67: 1.78 0.88 0.31 0.77 1.22 f0 111 185 4 18 17.6 +58 17 19 18.03 3.60 2.55: 1.89 1.00 0.39 0.81 1.35 b9:: 3.22 186 4 18 17.6 +58 25 50 17.20 3.00: 2.17 1.00: 0.42 0.83 1.26 g1 IV 1.79 3250 187 4 18 17.7 +58 19 32 16.08 4.97 4.13: 2.92 1.26 0.49 1.15 1.83 k0 III 2.00 4740 188 4 18 17.7 +58 23 19 14.63 3.30 2.52 1.63 0.77 0.27 0.69 0.97 a9 V 1.83 1100														
184 4 18 17.6 +58 16 05 17.79 3.71 2.67: 1.78 0.88 0.31 0.77 1.22 f0 III 2.04 7410 185 4 18 17.6 +58 17 19 18.03 3.60 2.55: 1.89 1.00 0.39 0.81 1.35 b9: 3.22 186 4 18 17.6 +58 25 50 17.20 3.00: 2.17 1.00: 0.42 0.83 1.26 g1 IV 1.79 3250 187 4 18 17.7 +58 19 32 16.08 4.97 4.13: 2.92 1.26 0.49 1.15 1.83 k0 III 2.00 4740 188 4 18 17.7 +58 23 19 14.63 3.30 2.52 1.63 0.77 0.27 0.69 0.97 a9 V 1.83 1100														
185 4 18 17.6 +58 17 19 18.03 3.60 2.55 1.89 1.00 0.39 0.81 1.35 b9: 3.22 186 4 18 17.6 +58 25 50 17.20 3.00 2.17 1.00 0.42 0.83 1.26 g1V 1.79 3250 187 4 18 17.7 +58 19 32 16.08 4.97 4.13 2.92 1.26 0.49 1.15 1.83 k01II 2.00 4740 188 4 18 17.7 +58 23 19 14.63 3.30 2.52 1.63 0.77 0.27 0.69 0.97 a9 V 1.83 1100												f0 III 01	2.04	7410
186 4 18 17.6 +58 25 50 17.20 3.00: 2.17 1.00: 0.42 0.83 1.26 g1 IV 1.79 3250 187 4 18 17.7 +58 19 32 16.08 4.97 4.13: 2.92 1.26 0.49 1.15 1.83 k0 III 2.00 4740 188 4 18 17.7 +58 23 19 14.63 3.30 2.52 1.63 0.77 0.27 0.69 0.97 a9 V 1.83 1100														
187 4 18 17.7 +58 19 32 16.08 4.97 4.13: 2.92 1.26 0.49 1.15 1.83 k01II 2.00 4740 188 4 18 17.7 +58 23 19 14.63 3.30 2.52 1.63 0.77 0.27 0.69 0.97 a9 V 1.83 1100														3250
188 4 18 17.7 +58 23 19 14.63 3.30 2.52 1.63 0.77 0.27 0.69 0.97 a9V 1.83 1100														
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				_										

Table 3. Continued

.T.S	ible 3.	Continued											
No.	RA(2000)	DEC(2000)	\overline{v}	U-V	P-V	X-V	Y-V	Z-V	V-S	V-I	Photom.	A_V	d
	hm s	0 1 11	mag	mag	mag	mag	mag	mag	mag	mag	sp. type	mag	рc
100	4 19 17 0	150 11 40	15.50	0.70	0.75.	1.00	0.89	0.29	0.79	105	fo IV	2.20	4770
190 191	4 18 17.9 4 18 17.9	+58 11 40 +58 20 40	17.78 16.02		2.75: 2.61	1.58	0.74				a3 IV		3880
192	4 18 17.9	+58 22 18	17.18		2.68		0.88		0.78				2790
193	4 18 18.0	+58 10 19	17.71		2.83::	2.12:		0.32	1.00	1.47	f7 V		2230
194	4 18 18.0	+58 24 35	17.09		2.88:						g7 V:	1.34	
195	4 18 18.1	+58 15 22	18.37				0.96				0.		
196	4 18 18.1	+58 07 19	15.37		3.73		1.19				g6 III	1.98	3200
197	4 18 18.1	+58 11 25	17.79	3.68		1.98	0.97	0.32	0.84	1.29	ři V-III	2.39	3240
198	4 18 18.2	+58 08 18	17.25		2.73:	1.97	0.95	0.31	0.95	1.37			
199	4 18 18.2	+58 14 23	17.39	4.31		2.57	1.10		1.08			1.67	730
200	4 18 18.3	+58 09 09	17.59		2.78:						a3 V-III		5200
201	4 18 18.4	+58 10 35	17.23		2.82:						f6 V-IV		1960
202	4 18 18.5	+58 26 00		4.69:	3.95		1.19				k0.5 IV		1580
203	4 18 18.5	$+58\ 19\ 07$	18.30	4.06:		2.24:	1.09:	0.45			f1 V-III		3090
204	4 18 18 6	+58 19 54	15.91	4.49::	4.06	2.86	1.05	0.63			k5 V:	1.05	340
205	4 18 18.7	+58 11 02		3.44			1.00		0.89			0.07	1000
206	4 18 19.1		15.91			2.91	1.24	0.48	1.19	1.86	g9.5 III		4200
207	4 18 19.3	+58 07 43	17.16		2.61:						a7 V-III		3690
208 209	4 18 19.4 4 18 19.6	+58 26 19	16.96		3.17:						g1.5 III f9 V-IV		6780 2120
210	4 18 19.6	+58 07 02 +58 23 01	17.56 14.61	2 10	2.18						a1.5 III	1.67	
211	4 18 20 1	+58 14 32	17 02	3.67:	2.10	1.23	0.84						3530
212	4 18 20.1		17.57	3.48	2.03	1.87	0.96	0.32	0.85	1.30	ev.		3070
213	4 18 20.3	+58 06 41	16.30	0.40		1.49		0.24	0.64	1.01	a2 V-III		3810
214	4 18 20.5	+58 23 31	18.20		2.02						g6 V-III		2110
215	4 18 20.7	+58 10 15		4.24	3.58						k1.2 V	1.65	
216	4 18 20.8	+58 21 17	16.96		2.43	1.37	0.66				a1.5 V		6040
217	4 18 20.8	+58 17 55	15.82		2.54			0.27	0.65	1.06	a1.5 V-III	2.29	3060
218	4 18 20.8	+58 11 48	17.89			2.42	1.08	0.41	1.01	1.46	g6 IV a9 V		3840
219	4 18 20.9	+58 15 34	17.79	3.67	2.74:	1.85	0.96	0.35	0.80	1.25	a9 V		3600
220	4 18 20.9	+58 20 44	17.19	3.53				0.28	0.64	0.98	a4 V-III	2.09	4990
221	4 18 21 1	+58 26 02	18.09			1.75:	0.76:	0.26:	0.73:	1.16			
222	4 18 21.3	+58 08 24	15.66		3.87		1.26	0.43	1,15	1.84	g6 III g2 IV a3 IV	2.26	3210
223	4 18 21.4	+58 18 53	16.34	3.86:	3.12	2.23	1.04	0.40	0.95	1.47	g2 IV	1.92	2010
224	4 18 21.4	+58 13 38	16.48	3.64 3.41::	2.67	1.61	0.78	0.28	0.64	1.00	a3 IV	2.29	4550
225	4 18 21.5	+58 24 20	17.79	3.41::	2.52:	1.82:	0.90:	0.31:	0.77:	1.16:			
226	4 18 21 6	+58 13 25		3.77:	2.78	1.72	0.85	0.30	0.76	1.17	a3 IV	2.57	
227	4 18 21.7	+58 18 59	18.22:		2.67:						f1 V-III		4430
228	4 18 21.9	+58 16 44	15.76		2.66				0.73		a8 III	2.00	3270
229 230	4 18 21.9 4 18 22.0	+58 16 01 +58 15 03	17.78		2.64: 2.68:		$0.88 \\ 0.86$				a8 V-III	9.96	4460
231	4 18 22 4	+58 04 50	17.88 17.54		2.00						f6 V-III		2290
232	4 18 22.5	+58 15 59		3.79:	2.05	2.00:	1.04	0.37	0.03	1.50.	f4 V		1630
233	4 18 22.7	+58 15 05	16.06		2.74	1 73	1.04 0.84	0.31	0.51	1.02	04 V		2540
234	4 18 22.9	+58 18 45	14.20		4.11	2.88	1 24	0.49	1.10	1.73	k0.5 III	1.75	
235	4 18 23.0	+58 23 12	17.40	-2.50	7.11	2.43	1.03				k0.7 V	1.57	
236	4 18 23.0	+58 14 52	17.35	3.63	2.74			0.34				2.30	
237	4 18 23.0	+58 08 25	17.06	3.00	2.85		0.99	0.31	0.07	1 42	F1 W_III	2.56	
238	4 18 23.4	+58 08 58	16.56	3.72:	2.89		0.99	0.32	0.92	1.39	f2 V	2.47	
239	4 18 23.7	+58 12 04	17.26		3.04:			0.37	0.94	1.43	f9.5 IV	2.08	
240	4 18 23.7	+58 28 38	17.90:				0.94:						
241	4 18 24.0	+58 19 12	17.31		2.63	1.89		0.34				1.73	2420
242	4 18 24.0	+58 16 48	16.75	3.53	2.55						a3 V-IV	2.15	
243	4 18 24.0	+58 24 48	17.99				0.97:				f1 V-III		3710
244	4 18 24.1	+58 15 58	18.10				1.20				f2 V-III:		2270
24 5	4 18 24.2	+58 16 39	17.42	3.54	2,65		0.82					2.15	4490
246	4 18 24.3	+58 24 13	17.74								k0 III	2.01	
247	4 18 24.9	+58 23 39	17.61		2.49:			0.28				1.63	
248	4 18 24.9	+58 15 02	14.76		4.43						k1.2 III	1.95	
249	4 18 25.1	+58 14 51	16.82				0.82				a3 V-III	2.45	
250	4 18 25.2	+58 19 20	18.02			1.64	0.88				a1.5 V::	2.52	
251	4 18 25.3	+58 24 39	14.39		4.14		1.26				k0 III	2.00	
252	4 18 25.7	+58 23 25		3.28:							f1 V	1.87	
253	4 18 25.8	+58 09 22	16.20		3.88:	2.74	1.20	0.44	1.14	1.77	g8 III	1.99	4820

Table 3. Continued

1,8	mie 9° (Jonannaea								
No.	RA(2000)	DEC(2000)	V U-V	P-V X-V	Y-V	Z– V	V– S	V-I Photom.	A_V	d
-,	hm s	0 1 11	mag mag	mag mag	mag	mag	mag	mag sp. type	mag	рc
					0.05		0.74	1 17 -73/ TV.	0.00	2510
254	4 18 25.8	+58 10 03	17.21 3.56	2.81 1.76	0.85 0.87	0.29 0.30	0.74	1.17 a7 V-IV: 1.22 a7 IV		3510 5410
255	4 18 25.9	+58 11 44	17.60 3.70 17.74 3.69	2.77: 1.79 2.58: 1.75	0.88			1.18 b9 V-III:		7010
256	4 18 26.2 4 18 26.2	+58 13 40 +58 15 01	16.14 3.84	2.80 1.78		0.30	0.71	1.13 a4 V		2500
257 258	4 18 26.3	+58 25 21	18.08:					1.28: g2.5 III	0.77	
259	4 18 26.5	+58 26 31	18.01:		0.96:					
260	4 18 26.6	+58 20 45	16.33 3.57:			0.28		0.92 a3 IV		4640
261	4 18 26.6	+58 12 14	18.28 3.72		: 0.98	0.31		1.45 f9 V:		2640
262	4 18 26.6	+58 24 24	16.90 3.43:	2.53 1.62				0.90 a6 V		3950
263	4 18 26.6	+58 05 36	14.84 3.30	2.53 1.72				1.13 fl V		1080
264	4 18 26.9	+58 18 10	17.98 3.51	2.67: 1.96		0.35	0.85	1.32 f4 V 1.29 f6 IV	1.77	3320 3410
265	4 18 27.0	+58 20 33	17.00 3.40 16.66 3.60	2.67 1.88 2.66 1.62		0.29	0.64	1.01 a4 V-IV	2.22	
266 267	4 18 27.0 4 18 27.0	+58 20 14 +58 24 45	15.93	4.09: 2.91		0.51		1.84 k0.5 IV		1400
268	4 18 27.1	+58 18 34	18.10 3.46	2.58: 1.78		0.33		1.19 fl V		4370
269	4 18 27.1	+58 10 04	14.12 3.36	2.54 1.56	0.73	0.26	0.60	0.93 a5 V	1.88	1220
270	4 18 27.2	+58 24 05	18.03	2.93:: 2.15	: 0.97:	0.40:	0.93:	1.35 g1.5 V		2190
271	4 18 27.4	+58 13 02	18.09	2.79	: 1.23	0.51	1.12	1.79 k0.5 V		880
272	4 18 27.6	+58 16 31	17.23 3.89		1.01	0.40	0.95	1.45 g6 IV		3300
273	4 18 27.6	+58 10 36	17.85 3.82	2.29		0.39		1.49 g0 V-IV		1830 3280
274	4 18 27.7	+58 15 23	18.11 3.60	1.98 2.60 1.60		0.33	0.92	1.36 f4 V 0.98 a4 V		3300
275	4 18 27.7 4 18 27.8	+58 16 48 +58 04 56	16.33 3.54 18.36		0.77				2.18	
276 277	4 18 28.0	+58 18 20	17.39:	2.76 1.79				1.16 a6 V	2.43	
278	4 18 28.1	+58 14 42	16.94 3.76	2.86 2.04				1.44 f2 V		1940
279	4 18 28.2	+58 07 56	15.48 3.56	2.68 1.86	0.94	0.31	0.86	1.34 f1 V	2.22	1210
280	4 18 28.2	+58 16 03	17.60 3.51	2.57 1.66		0.30	0.73	1.14		
281	4 18 28.2	+58 22 02	18.24		0.94	0.39	0.85	1.36: g9 V		1870
282	4 18 28.3	+58 12 15	17.46	2.77: 1.76		0.32	0.73	1.12 a5 V-III		4470
283	4 18 28.5	+58 03 36	16.17	2.63 1.85				1.30 f2 V		1690 4460
284	4 18 28.6 4 18 28.7	+58 03 50 +58 28 28	17.46 16.17 18.08 18.16:		: 0.82:			1.24: f4 V-III	1.50	4400
285 286	4 18 28.7	+58 28 28 48 +58 13 39	13.22 3.58	3.05 2.02	0.82	0.35	0.30	1.09 g9 III	0.14	2920
287	4 18 28.9	+58 16 55	16.62 3.58	2.65 1.62	0.77	0.29	0.64	1.00 a4 V-III		3680
288	4 18 29.2	+58 18 01	18.05	2.60: 1.84		0.33	0.77	1.20		
289	4 18 29.8	+58 07 12	17.77:		: 1.03	0.38		1.46 g0 V-III		1940
290	4 18 30.0	+58 19 17	14.50 5.85:		1.49			2.18 k1.5 III		1720
291	4 18 30.1	+58 22 38	17.59 3.24::					1.18 f5 IV	1.60	4990
292	4 18 30.1	+58 07 54	17.76	2.60: 1.53	1.00			1.46: 0.93 a1.5 V	2 20	7470
293	4 18 30.3 4 18 30.5	+58 20 39 +58 27 30	17.76 3.57 16.08 3.52	2.89 2.09				1.22 g4 V	1.47	
294 295	4 18 30.6	+58 10 21	16.73 3.84	2.93 1.83				1.21 a4 V-III		3130
296	4 18 30.6	+58 28 33	17.54	2.53				1.42 k2.2 V	1.41	860
297	4 18 30.8	+58 14 53	16.05 3.63			0.31	0.76	1.19 a7 V	2.38	1970
298	4 18 31.0	+58 13 52	18.18	1.90		0.31	0.83	1.27	_	
299	4 18 31.1	+58 10 28	16.88	2.99		0.49		2.03 g5.5 III	2.78	4400
300	4 18 31.1	+58 13 59	18.15	1.85		0.31	0.82		0.00	5040
301	4 18 31.4	+58 11 30	17.38 3.83	2.81 1.74 2.59 1.60		0.31 0.29		1.10 a2 V-III 1.00 a4 V		5040 3520
302	4 18 31.5 4 18 31.5	+58 18 30 +58 12 58	16.49 3.59 14.78 3.53	2.59 1.60 2.82 1.98		0.34		1.23 g1.5 IV		1240
303 304	4 18 31.5	+58 12 58	15.49 3.31	2.58 1.83		0.32		1.19 f6 IV		1840
305	4 18 31.8	+58 03 33	16.84	2.73: 1.98		0.38		1.29 f8 IV		3080
306	4 18 31.9	+58 19 37	17.53 3.58	2.76 1.74		0.33		1.12 a6 V		4500
307	4 18 32.1	+58 12 21	17.79 3.50	2.76: 1.82	0.88	0.32	0.74	1.15 a9 V		3980
308	4 18 32.1	+58 11 23	15.54 4.61	3.79 2.67		0.44	1.08	1.73		
309	4 18 32.2	+58 14 11	16.22 3.88	2.85 1.84		0.31		1.28 a5 V-IV		2280
310	4 18 32.4	+58 05 54	17.69		0.86	0.26		1.28 f9 V-III		2750
311	4 18 32.8	+58 18 07	14.42 3.36	2.58 1.83		0.33		1.23 f3 V 1.14 b9.5 V	1.86	750 5730
312	4 18 32.8	+58 13 39 +58 17 10	17.43 3.76 16.09 3.54	2.73: 1.79 2.61 1.59		0.34 0.29	0.73	1.14 by.5 v 1.02 a4 IV		3730
313 314	4 18 32.9 4 18 32.9	+58 23 53	15.35 4.94:	4.12 2.89		0.49	1.09	1.72 k0.7 III		3910
315	4 18 32.9	+58 14 21	15.78 3.66	2.61 1.48		0.25		1.04 a2 V-III:		2830
316	4 18 33.0	+58 25 05		3.61: 2.64		0.46		1.67 g9.5 V	2.18	495
317	4 18 33.0		17.84 3.69	2.78: 1.91		0.33		1.31 f4 III	1.95	6470

Table 3. Continued

Ta	ible 3. (Continued										
No.	RA(2000)	DEC(2000)	V U-V	P-V	X-V	Y-V	Z-V	V-S	V-I	Photom.	A_V	
	hm s	0 1 11	mag mag							sp. type	mag	рс
318	4 18 33.0	+58 27 16	17.94:	2 44	1.80:	1.01.	O 30:	0.74	1 12			
319	4 18 33.1	+58 18 18	17.92		1.93					a5 V	2.79	4630
320	4 18 33.2	+58 28 26	17.80	2.54:	1.69:							
321	4 18 33.3	+58 22 17		2.49						f3 III:		5390
322	4 18 33.4	+58 22 23 +58 22 55	15.68 3.54	$\frac{2.81}{3.98}$	2.01	0.93 1.21				g0 IV k0 III		1820 2000
323 324	4 18 33.6 4 18 33.6	+58 17 09	13.94 4.81 18.19	0.90		0.94					1.69	2000
325	4 18 33.7	+58 18 30	14.60 6.34	5.36		1.51				k4 III		2670
326	4 18 33.7	+58 14 48	15.56 3.80	2.74						a4 IV		2510
327	4 18 33.9	+58 24 43	17.41 3.60::							f0 V-IV:		3270
328 329	4 18 34.1 4 18 34.2	+58 19 28 +58 11 27	14.91 3.50 16.60 3.69		$\frac{2.02}{2.20}$	$0.91 \\ 0.97$	0.35			g1 IV k0 V	1.47	1320 800
330	4 18 34.3	+58 14 33	17.07 3.56	2.83			0.35			f7 IV		3090
331	4 18 34.4	+58 18 41	15.86 4.30		2.43:		0.39			g6 III:		4480
332	4 18 34.4	$+58 \cdot 16 \cdot 33$	17.10 3.55:		1.64			0.65	1.01	a4 V-III	2.22	
333	4 18 34 4	+58 24 40	16.93 3.61:		1.96	0.95				f3 IV	2.13	3060
334 335	4 18 34.5 4 18 34.7	+58 15 28	15.38 4.62	3.79 2.67:	2.70	0.85		1.07		f4 [[]:	1 55	8970
336	4 18 34.7	+58 15 51 +58 10 06	18.15 3.29 17.67 3.62	2.68:		0.98	0.34			f2 V:		2960
337	4 18 34.8	+58 19 20	16.26 3.50		1.96	0.93	0.35			f9 IV		2350
338	4 18 34.9	+58 19 45	15.22 4.57		2.65	1.18	0.44	1.05	1.66			
339	4 18 35.1	+58 18 27	11.80 5.16		2.97	1.15	0.52			k3.7 III		1500
340	4 18 35.3	+58 16 53	15.46 3.77		1.86	88.0	0.33			a8 V		1340
341 342	4 18 35.4 4 18 35.5	+58 15 22 +58 11 17	18.02 17.49 3.68	2.75: 2.82	1.87	0.97 0.87	0.33				3.46	3790
343	4 18 35.5	+58 12 26	16.59 3.70	2.75		0.79	0.29			a4V		3380
344	4 18 35.6	+58 19 02	18.12 3.60	2.75:		0.91	0.34	0.77	1.19	a9 V-IV		4430
345	4 18 35.7	+58 24 09	17.26	2.88:		0.97	0.35	0.91	1.37	f1 V-III		2350
346	4 18 35.7	+58 09 03	17.65		3.10:					m2 V-III::		
347	4 18 36.1	+58 20 33	16.73 3.66	3.00		0.96				g4 IV	1.48	2860
348 349	4 18 36.2 4 18 36.3	+58 16 34 +58 09 02	17.38 3.43: 17.77	2.03	2.46	0.52 1.09	0.32 0.37	0.69		g2.5 III	2.07	8800
350	4 18 36.4	+58 24 37	17.41	2.64:						a5 V-III		5010
351	4 18 36.6	+58 25 36	16.80		2.98	1.34:	0.53	1.15	1.87	k0 IV	2.51	1730
352	4 18 36.6	+58 17 19	17.65 3.66	2.76		0.94	0.34					3250
353	4 18 36.7	+58 16 54	16.28 3.62	2.59		0.77		0.64				3370
354 355	4 18 36.7 4 18 36.7	+58 13 13 +58 22 17	17.46 3.60 15.86	$\frac{2.75}{3.99}$	$\frac{1.79}{2.84}$	$0.85 \\ 1.25$	0.50			a7 V g9 III	1.99	3920 4200
356	4 18 37.1	+58 22 38	17.52	2.91:		0.98				glIV	1.64	
357	4 18 37.2	+58 11 25	17.75 3.77	2.86:		0.87	0.29	.0.75	1.16	a7 V-IV		4110
358	4 18 37.2	+58 14 39	18.01 3.87		2.25	1.05	0.37					
359	4 18 37.3	+58 14 09	17.94		1.83	0.87	0.30			1 17		400
360 361	4 18 37.3 4 18 37.4	+58 25 43 +58 18 09	16.10 4.47: 17.63 3.61	3.92: 2.69:		0.87	0.58			k4.5 V a8 V		408 3970
362	4 18 37.5	+58 12 53	16.72 3.64		1.68	0.79				a6 III	2.16	
363	4 18 37.7	+58 12 24	16.07 3.74	2.73		0.83		0.69	1.10	a5 V	2.35	
364	4 18 37.8	+58 24 30	17.90		2.87:	1.02:	0.55	1.14	1.69	k5.5 V	88.0	840
365	4 18 37.9	+58 21 20	16.49 3.29			0.86	0.33			f4 IV	1.66	
366	4 18 37.9	+58 14 14	16.00 4.66	3.84		1.25	0.46			g6 III	2.21	
367 368	4 18 37.9 4 18 37.9	+58 09 57 +58 08 10	16.87 3.67 17.25	2.74 2.76:		0.80	0.27			a3 IV a3 V-III	2.38	5230 4590
369	4 18 38.0	+58 17 40	16.71 3.43	2.75	1.90		0.35	0.84	1.35	g0 IV	1.45	
370	4 18 38.0	+58 15 46	16.80 3.48	2.57		0.75	0.27	0.61	0.97	a4 V-III	2.05	
371	4 18 38.1	+58 26 45	17.81	2.79:	1.82		0.34	0.69:	1.06	b9.5 V	3.20	6480
372	4 18 38.2	+58 07 13	18.25	0.01		0.86		0.83		10.537	1.00	000
373 374	4 18 38.2 4 18 38.2	+58 24 21	17.32 3.96::	3.34: 2.76:		1.01: 0.90				k0.7 V	1.36	
374 375	4 18 38.2	+58 14 05 +58 16 27	17.49 15.97 3.55	2.76:						a9 III a7 IV	2.20 2.11	
376	4 18 38.3	+58 19 44	17.60 4.06	2.00	2.35	1.04	0.40	1.00	1.47	g6 IV	1.81	
377	4 18 38.4	+58 26 25	17.90	2.72::	1.84:		0.25:	0.91:	1.35	a9:	2.40	
378	4 18 38.4	+58 21 32	17.93 3.43		1.92:	0.86	0.31	0.88	1.38	g3 V	1.32	
379	4 18 38.5	+58 16 34	16.44 3.59:	2.58						a8 III	1.92	
380	4 18 38.5	+58 14 11	18.07	9.57	2.07	0.93:	0.33	0.96	1.42	g0 V	1.77	
381	4 18 38.6	+58 19 16	10.70 3.51	2.57	1.05	0.80	0.29	0.72	1.13	WL IA	2.02	4200

Table 3. Continued

16	mie a. (Jonanna										
No.	RA(2000)	DEC(2000)	V = U							Photom.	A_V	d
	hm s	0 / //	mag m	ag mag	mag	mag	mag	mag	mag	sp. type	mag	рc
382	4 18 38.7	+58 13 39	16.52 3.	96: 3.16	2.31	1.05	0.38	0.99	1.46	g1.5 III	1.83	5470
383	4 18 38.8	+58 15 01	16.83 3.		1.67	0.81	0.31	0.63	0.99	a5 V-III		3730
384	4 18 38.9	+58 15 10	16.84 3.		1.71	0.83	0.22			a5 V-III		3550
385	4 18 39.0	+58 14 55	16.04 3.		1.63	0.81	0.29			a2 V-III		2980
386	4 18 39.1	+58 12 43	17.93 3.1		2.32:	1.18	0.39 0.43			g0V-IV		1900 4250
387	4 18 39.2 4 18 39.2	+58 11 51 +58 16 53	15.93 4.4 17.35 3.4		2.60 1.68	0.83	0.43			g6 III a7 V		4030
388 389	4 18 39.3	+58 14 03	16.02 4.		2.68	1.23	0.44			g6 III		4060
390	4 18 39.5	+58 07 38	16.39		1.94	0.94		0.86			2.21	
391	4 18 39.8	+58 27 03	17.13 3.		1.90	0.92				f4 V:	1.94	
392	4 18 39.8	+58 11 29	18.06 3.		1.97	0.93				f3 V-IV	2.13	
393	4 18 39.9	+58 20 26	16.61 3.0		1.75	0.85	0.32			a7 IV	2.25	
394	4 18 40.0	+58 14 51	17.56 3.		1.88 1.82	$0.91 \\ 0.89$	$0.34 \\ 0.29$			f1 V f2 III:	1.92	3240
395 396	4 18 40.1 4 18 40.2	+58 14 29 +58 22 04	17.85 3.1 17.63		2.09	0.09	0.38			f9 IV		4060
397	4 18 40.3	+58 15 54	13.27 3.4		2.22	0.96	0.38			g8 IV	1.22	
398	4 18 40.4	+58 17 47	18.11		1.77	0.93	0.32			al.5 V-III		
399	4 18 40.5	+58 23 56	14.59 3.		1.74	0.81	0.29			f8 IV		1380
400	4 18 40.7	+58 19 26	17.89 3.		1.79	0.88	0.32	0.74				4080
401	4 18 41.0	+58 12 52		3.57 2.71:	1.79	0.89	0.29			a9 V-IV	2.22	
402	4 18 41.2	+58 16 53	17.59 3.	57 2.58 #4 2.50	1.68 1.56	0.87 0.75	$0.29 \\ 0.28$			b9.5 V a4 V	2.84 2.10	
403 404	4 18 41.3 4 18 41.3	+58 19 10 +58 08 56	16.11 3.1 16.66 3.1	47 2.00	1.96	0.94	0.32	0.87			2.05	
405	4 18 41.5	+58 08 18	16.74 3.		1.67	0.78	0.27	0.64			2.00	
406	4 18 41.7	+58 09 48	17.09 3.0		1.71	0.81	0.28			a5 V-III	2.29	3980
407	4 18 41.8	+58 13 26	16.37 4.	84 3.95:	2.85	1.33	0.46	1.20				
408	4 18 41.8	+58 16 07	17.17 3:	51: 2.59	1.73	0.84				a9 V		3180
409	4 18 41.8	+58 17 52	17.12		2.65		0.49			g9.5 V	2.21	660
410	4 18 41.9	+58 17 58	18.03 17.91			1.05: 1.20	0.37			f9 V-IV k5 V	1.67	2170 640
411 412	4 18 41.9 4 18 41.9	+58 16 04 +58 11 55	17.91 17.36: 3.4	51 280	1.95	0.95	0.38		1.30	KO V	1.07	040
413	4 18 42.2	+58 14 35	16.61 3.		1.70	0.78	0.30	0.67		a6 III	2.18	5180
414	4 18 42.3	+58 08 58	17.55		1.59	0.75	0.24			a3 V-III		6160
415	4 18 42.3	+58 14 11	17.44 3.	71 2.73	1.61	0.77	0.27			a2 V-III	2.44	5750
416	4 18 42.4	+58 10 53	16.18 3.		1.94	0.94		0.85				1360
417	4 18 42.4	+58 27 40	16.48 3.		1.59	0.76				a5 V-III	2.06	
418	4 18 42.5	+58 09 36	13.79 4.5		2.89	1.25 0.87	$0.49 \\ 0.31$			k0.7 III	1.70	1900
419	4 18 42.5 4 18 42.6	+58 13 17 +58 18 03	17.93 16.52 3.3		: 1.91 2.18			08.0		g4 IV		2380
420 421	4 18 42.6	+58 24 55	17.48		2.21:						2.41	
422	4 18 42.6	+58 16 12	15.54 4.		2.63	1.19		1.05				
423	4 18 42.7	+58 11 06	16.25 3.		1.70	0.89	0.32			a0.5 V	2.78	
424	4 18 42.8	+58 15 58	17.90 3.4		1.81	0.86		0.73			2.07	
425	4 18 42.8	+58 16 56	18.08 3.4	57	1.84	0.90	0.35	0.79				4250
426	4 18 42.8	+58 17 58	18.33	0.04	1.85:		0.34			a5 V-III	2.60	6100
427	4 18 42.8	+58 13 25	17.60		$\frac{1.91}{2.66}$	$0.91 \\ 1.22$	$0.30 \\ 0.44$	0.84 1.09		g5.5 III	2.13	2570
428 429	4 18 42.9 4 18 42.9	+58 17 12 +58 13 51	15.77 4.0 15.94 4.1		2.65	1.24		1.18	1.87	80.0111	2.10	0010
429	4 18 42.9	+58 24 49	15.12 3.		1.77	0.81		0.75		f5 V	1.50	1060
431	4 18 43.1	+58 14 43	17.43 3.0		1.79	0.85				a7 V	2.31	
432	4 18 43.1	+58 14 58	17.62 3.4	49 2.68	1.82	0.85	0.31	0.72	1.13	f0 V	2.10	3660
433	4 18 43.4	+58 16 38	14.81 3.		1.59	0.74	0.27	0.62		a7 V	1.87	1410
434	4 18 43.4	+58 14 32	16.28 2.9		1.31	0.66	0.25	0.55		£4 3 7 7 7 7 7	0 1 1	
435	4 18 43.4	+58 13 22	17.97		1.85	0.90	0.29			f1 V-III	2.14	3950
436	4 18 43.4	+58 19 19 +58 25 52	18.42 4.6 15.47 4.6		2.44	0.87: 0.93	0.33	0.73		k3 V	0.96	381
437 438	4 18 43.5 4 18 43.5	+58 25 52	18.16 3.3		1.85	0.99	0.33	0.79	1.28	NO Y	0.80	001
439	4 18 43.6	+58 15 04	17.58		1.96		0.34			f2 V	2.28	2890
440	4 18 43.7	+58 26 32	17.74							g9.5 IV	1.04	
441	4 18 43.8	+58 14 16	17.23 3.0	66 2.67	1.71					a0 V-III	2.78	
442	4 18 43.8	+58 27 37	18.07:			0.97:	0.43:	0.82:	1.27		1.22	1700
443	4 18 43.8	+58 11 31	18.09 3.4		1.87	0.92		0.76				
444	4 18 44.0	+58 22 37	17.25 3.3		1.65	0.78	0.31			a8 V	1.92	
445	4 18 44.0	+58 16 13	17.81 3.8	57 2. 69:	1.79	0.86	0.30	U.75	1,14	ay v	2.20	3990

Table 3. Continued

10	able 5. (Jonumaeu										
No.	RA(2000)	DEC(2000)	V U-V	P-V	X– V	Y-V	Z– V	V– S	V– I	Photom.	A_V	d
	hm s	0 1 11	mag mag	mag	mag	mag	mag	mag	mag	sp. type	mag	рc
116	4 18 44.0	+58 13 02	16.05 4.62	2 04	2.75	1.25	D 44	1 19	1 76	g6 III	2 20	3930
446 447	4 18 44.0	+58 28 29	18.06	3.84		0.90					2,20	0000
448	4 18 44.2	+58 13 21	16.94 3.77	2.82						a7 V-III	2.51	2790
449	4 18 44.3	+58 15 27	16.86 3.53	2.64	1.76		0.30				2.13	2670
450	4 18 44.3	+58 26 29	17.95	2.65:	1.95:						.1.72	3010
451	4 18 44.7	+58 16 33	15.88 3.58		1.68		0.27					2500
452	4 18 44.7	+58 15 57	15.81 3.76		1.82					fO III		2890
453	4 18 44.8	+58 15 00	17.19 3.57	2.66						a6 IV		5270
454	4 18 45.1	+58 06 06	18.03							f6 V-III		3200
455 456	4 18 45.3	+58 09 56 +58 15 27	17.77 3.78 16.71 3.45	2.58	2.23	1.00 0.81		0.69		g2 III	2.02	2910
457	4 18 45.4 4 18 45.5	+58 10 06	17.17 3.57	2.85		1.02				f7 IV		3240
458	4 18 45.6	+58 12 25	17.06: 3.84	2.85		0.92	0.31	0.77		-,	1.00	02.0
459	4 18 45.7	+58 19 37	18.07 3.39		1.83	0.85		0.78		f2 V	1.92	4260
460	4 18 45.8	+58 17 17	17.73 3.64		1.78	0.88		0.79			2.39	4240
461	4 18 45.9	+58 13 39	15.90 4.51:	3.72	2.65	1.22	0.45			g8.5 IV		1330
462	4 18 46.0	+58 24 49	17.23 3.43:	2.73:		0.89	0.33	0.91				1770
463		+58 16 06	17.20 3.47	2.69		0.88		0.74				3070
464		+58 20 56	16.47 4.61		2.70	1.02				k4 V:		464
465		+58 15 14	15.88 4.48	3.65 2.60	2.60	1.18				g6 III f2 III		4150 4230
466 467	4 18 46.4 4 18 46.5	+58 25 02 +58 13 34	16.57 3.56: 17.42		2.18	1.01				f9 V-IV		1770
468		+58 14 24	15.88 3.62		1.65	0.81	0.31	0.65				2550
469		+58 14 17	17.00 3.63:		1.67	0.83		0.68				3930
470		+58 14 57	16.01 3.69	2.72	1.83	0.87				f2 III		3020
471	4 18 46.7	+58 17 51	16.15 3.69		1.68	0.81	0.30	0.70	1.09	a4 IV	2.34	3490
472	4 18 46.7	+58 20 28	17.71 3.52	2.62	1.91	0.89				f7 III		6730
473	4 18 46.8	+58 15 48	15.88 3.77	2.72	1.78	0.87	0.31			a9 III		3090
474	4 18 46.9	+58 13 37	16.42 3.73:	2.66	1.63	0.80	0.25			a3 V-III		3380
475	4 18 47.0	+58 12 55	18.54	0.00	1.99:		0.33 0.28			g6 V		2670 4270
476 477	4 18 47.0 4 18 47.1	+58 15 16 +58 21 45	16.99 3.50: 14.71 3.18	2.69 2.57	1.65	0.81				a4 V: g1 IV		1490
478		+58 16 08	17.82 3.62		1.77	0.92	0.35			b9 V		7240
479	4 18 47.3	+58 14 57	16.64 3.59:	2.71		0.78	0.27	0.68				3530
480		+58 20 04	16.29 3.62		1.63	0.76				a3 IV		4200
481	4 18 47.3	+58 15 12	17.89	2.66:	1.80	0.95				b9 V:	3.15	7400
482		+58 14 53	17.12 3.73:	2.67	1.72 1.51	0.83		0.75				
483		+58 19 20	16.60 3.38	2.57	1.51	0.71				a4 V:		4180
484		+58 15 54	16.31		1.70	0.82				a3 IV		3780
485		+58 14 28	17.81		2.40	1.12				g2.5 III		9250
486 487	4 18 47.5 4 18 47.6	+58 16 42 +58 18 55	15.23 4.56 18.40 3.43	3.73		1.10 0.95	0.38	0.90		g8.5 III		3650 3240
488	4 18 47.6	+58 28 20	17.67	2.61						g1.5 V		2380
489	4 18 47.6	+58 16 45	15.99 3.72							a7 V-IV		1870
490		+58 15 58	14.70 3.92	3.06:	2.00:	0.97	0.34	0.90	1.48	a7 V-III	2.85	850
491	4 18 47.8	+58 26 11	17.71		2.03	0.96:	0.32	0.98:	1.44	g0 ∨		2180
492		+58 17 54	16.93 3.49:	2.70		0.95	0.35	0.85	1.31	f4 V		2030
493		+58 27 07	17.03 3.44:	2.68:						a8 V:		3230
494		+58 13 49	17.18		1.77					a8 III		5970
495		+58 09 29	16.57 3.58:		1.67	0.77				a4 V-IV:		3440 3340
496 497	4 18 48.3 4 18 48.5	+58 19 08 +58 13 26	15.83 3.62 18.17	≥.03	1.71 1.83	0.82 0.84	0.30			a9 III g0 V-III		3250
497	4 18 48.5	+58 12 58	18.17 3.81		2.11:		0.35		1.47			2970
499		+58 21 08	14.00	4,46	3.13	1.31	0.52			k1.7III		1990
500		+58 14 24	16.82 3.60		1.66	0.77				a5 V		3740
501	4 18 48.6	+58 13 48	15.72 4.52:	3.79						g7 III		3830
502		+58 16 41	16.60 3.76	2.72		0.81		0.68				
503	4 18 48.6	+58 14 36	15.60 4.39	3.54	2.54	1.16		1.05				
504		+58 22 21	16.56 3.88:	3.19	2.25	0.96	0.41			k0 V	1.31	740
505		+58 16 09	15.77 3.72	2.75	1.85	0.90	0.33			f1 III		2720
506		+58 29 28	16.57 3.17	2.47	1.82	0.86	0.37	0.73				1860
507		+58 16 20	15.74 3.14	2.24	1.32	0.67	$0.26 \\ 0.28$			a0 V		4150
508 509	4 18 49.0 4 18 49.0	+58 21 26 +58 21 09	14.90 3.23 12.93 3.24	2.43	1.56 1.55	0.76				a9V f0IV	1.59	1310 710
909	4 10 45.0	F00 21 U9	12.30 3.24	4.00	1.00	0.10	v.40	0.00	0.92	1014	1.00	, 10

Table 3. Continued

Ta	ibie 3. (Jonumuea										
No.	RA(2000)	DEC(2000)	V = U-V	P-V	X– V	Y-V	Z- V	V-S	V-I	Photom.	A_V	d
	hm s	0 / //	mag mag	mag	mag	mag	mag	mag	mag	sp. type	mag	рc
										40.7.7		
510	4 18 49.1	+58 17 03	17.60 3.66		1.93	0.95	0.36		1.32			3160
511	4 18 49.2	+58 13 25	15.78 3.84:		2.27	1.08	0.39 0.30	0.98		f9 V-IV a4 V-IV	2.31	730 3210
512	4 18 49.2	+58 16 55	16.49 3.70: 17.92 3.53		1.69 1.82	0.89		0.09				4090
513	4 18 49.3 4 18 49.4	+58 10 52 +58 12 18	16.56 3.67		1.69	0.80	0.29			a4 V-IV		3370
514 515	4 18 49.4	+58 13 41	16.88 3.60		1.80	0.87	0.32			a9 V		2570
516	4 18 49.5	+58 16 46	15.96 3.83	2.78	1.80	0.88	0.33			a8 III	2.29	3210
517	4 18 49.5	+58 28 00	18.07		2.43:	1,15:	0.54:	0.99:	1.46			
518	4 18 49.5	+58 19 09	18.14 3.53		2.00					f9 IV		5510
519	4 18 49.5	$+58\ 16\ 07$	15.43 3.69		1.64	0.80				a3 IV		2720
520	4 18 49.5	+58 22 44	15.35 3.49		1.93	0.92				f6 IV a5 V		1520 3840
521.		+58 13 10	17.08 3.72 14.99 3.67		1.75 1.70	$0.82 \\ 0.82$	0.29 0.30			a5 V a5 V-IV		1520
522 523	4 18 49.6 4 18 49.6	+58 14 03 +58 18 19	17.20 3.63		1.76	0.80	0.30	0.69		20 V-IV	2.20	1020
524	4 18 49.7	+58 17 25	15.68 4.68		2.72		0.45	1.10				
525	4 18 49.8	+58 26 13	17.26		1.92		0.36	0.81:	1.28	g1.5 V	1.29	1940
526	4 18 49.8	+58 10 32	15.63 3.38	2.61	1.80	0.89	0.31	0.80	1.20	f2 V	1.94	1370
527	4 18 49.8	+58 13 21	17.91		1.75	0.81	0.27	0.84				
528	4 18 49.9	+58 18 52	15.28 4.53		2.66	1.19	0.44	1.05	1.67	g6 III		3040
529	4 18 50.0	+58 08 56	15.59 3.53		1.95	0.94	$0.31 \\ 0.32$			f3 V a8 IV		1140 3710
530	4 18 50.0	+58 15 06 +58 14 23	16.77 3.60: 15.86 4.51:		1.73	0,86 1,16	0.32	1.09		ao I v	2.10	2110
531 532	4 18 50.2 4 18 50.3	+58 14 13	16.74 3.52:	2.61	1.64	0.81	0.27			a5 V-III	2.14	3640
533	4 18 50.3	+58 08 14	16.48 3.88		2.19	1.03				g0 IV		2090
534	4 18 50.3	+58 20 43	16.67 3.34		1.77	0.86	0.32			f4 IV		3290
535	4 18 50.3	+58 14 54	17.06 3.75		2.11	1.00	0.36			g0 IV		3010
536	4 18 50.4	+58 20 33	17.45 3.60		2.14	0.94	0.37			g6 V		1470
537	4 18 50.4	+58 08 47	17.57 3.54:			0.96	0.29			f4 V		2610
538	4 18 50.4	+58 10 03	17.44 3.72	2.93:	2.10 1.90:		0.35			f7 IV	2.18	3370
539 540	4 18 50.5 4 18 50.5	+58 28 07 +58 14 26	17.75 17.66		1.78					a8 V-III	2.30	3970
541	4 18 50.6	+58 15 31	16.02 3.51	2.52	1.48	0.71				a2 V-IV		3430
542	4 18 50.7	+58 16 43	17.50		1.84	0.85		0.76			1.97	
543	4 18 50.7	+58 17 38	16.59 3.69	2.66	1.68	0.81		0.71				
544	4 18 50.8	+58 13 18	18.26 3.53		1.82	0.94	0.34	0.82	1.29			
545	4 18 50.9	+58 14 23	17.31		1.77	0.81	0.30:	0.77	1.14	a6 V		3850
546	4 18 50.9	+58 15 52	15.68 3.77		1.68	0.82				a2 IV	2.58	2880
547	4 18 50.9	+58 11 44	17.69 2.92		1.78 1.73	0.90 0.85	0.36			f0 V	2.00	1790
548 549	4 18 51.0 4 18 51.1	+58 09 07 +58 16 39	15.97 3.40 15.56 4.63		2.73	1.22	0.44			III 8g		3690
550	4 18 51.1	+58 12 53	16.51 3.71		1.75	0.86	0.31			a6 V		2680
551	4 18 51.2	+58 17 08	16.98 3.76		1.75	0.82	0.31	0.67		a6 III		5840
552	4 18 51.2	+58 16 45	17.49		1.88	0.91	0.31	0.87		f5 III		5610
553	4 18 51.3	+58 16 50	16.60 3.68		1.66	0.80	0.30			a4 V		3430
554	4 18 51.3	$+58\ 15\ 05$	16.77 3.59		1.67	0.80	0.30			a5 V		3620
555	4 18 51.3	+58 14 19	15.08 4.64		2.79	1.14	0.38			g9.5 III		3410 2120
556	4 18 51.6	+58 17 01	17.90 16.14 3.79		$\frac{2.19}{1.87}$	$0.99 \\ 0.92$	0.38			gl V: fl III		3110
557 558	4 18 51.6 4 18 51.6	+58 14 41 +58 14 16	16.59	2.79		0.82	0.28			a9 III		4560
559	4 18 51.7	+58 05 50	17.48	2.00	2.07:		0.31	0.97	1.46		2.00	_000
560	4 18 51.7	+58 15 07	17.29 3.56:	2.66		0.77	0.30	0.69	1.06			
561	4 18 51.7	+58 23 44	17.52 3.41:	2.67:	1.77	0.91	0.37	0.73	1.19	a9 V		3590
562	4 18 51.7	+58 21 34	17.44 3.57	2.61	1.54	0.72	0.28			a2 V-III		6390
563	4 18 51.9	+58 20 38	16.50 3.13	2.26	1.31	0.64	0.25		0.74			4810
564	4 18 51.9	+58 15 14	15.98 3.53	2.63	1.63	0.81	0.29			a5 V-IV a4 V-III		2590 2890
565 566	4 18 51.9	+58 23 39 +58 12 01	16.14 3.62 17.94 3.59	2.04	1.64 1.81	0.79 0.86	0.28	0.67		a4 V-111 a8 V		4600
566 567	4 18 52.1 4 18 52.2	+58 12 01	16.22 3.77	2.77	1.78	0.86	0.31			a6 V-IV		2280
568	4 18 52.2	+58 07 43	15.21 3.62	2.86	2.06	0.99	0.34	0.88		f7 IV		1290
569	4 18 52.3	+58 28 09	14.58 4.90	4.04	2.90	1.24	0.50	1.09		k0 III		2510
570	4 18 52.4	+58 15 43	16.47 3.66	2.66	1.66	0.79	0.28			a4 V		3330
571	4 18 52.4	+58 19 36	17.02 3.56	2.77	1.97	0.97	0.37		1.35	f3 V		2150
572	4 18 52.5		16.87 3.67:		1.75	0.83	0.27	0.75		a6 V-III	2.35	3190
573	4 18 52.5	+58 21 00	16.63 3.28	2.49	1.67	0.85	0.27	0.77	1.15			

Table 3. Continued

Te	tore 3). C	OHU	nueu									_		
No.	RA(20	000)	DEC	(2000)	V	U-V	P– V						Photom.	A_V	d
	h m	8	0	1 11		mag	mag	mag	mag	mag	mag	mag	sp. type	mag	pc
	4.10		150	28 46	17 00		2 52.	1 84	0.86+	0.44	0.80:	1 10:	g1.5 V:	1.18	2640
574 575	4 18 4 18			28 49 14 47	18.01			1.97:	0.98	0.31	0.90	1.41			
576	4 18			16 16	16.62			1.67	0.78	0.29	0.65	1.00	a4 V	2.31	
577	4 18			13 50	15.84			1.77:	0.87	0.29:	0.63	1.24	a7 IV	2.38	2350
578	4 18			20 31	17.89		2.51:	1.72	0.89	0.28			61	1.00	
579	4 18			09 12	17.91		2.52:	1.69:	0.86	0.27	$0.80 \\ 1.04$		11	1.92	
580	4 18			14 21	15.06		3.51 2.96:			0.43			g5.5 V	1.47	1490
581 582	4 18 4 18			21 30 08 28	17.41 18.04	3.04	2.90:	1.92	0.98	0.28	0.96	1.45	f2 V-III:		
583	4 18			13 36	16.89	3.87	3.12						g0 IV	2.16	
584				15 13		3.61:	2.69	1.73	0.88	0.32	0.67	1.02	a6 V	2.28	
585	4 18		+58	12 27	17.50	4.90		2.93	1.32				g5.5 III	2.62	
586	4 18	52.9		11 27	16.10		2.68	1.62	0.80				a3 IV		3760
587	4 18			24 26	16.94			2.62	1.07		1.01	1.52	k3.5 V:	1.28	600 3660
588	4 18			15 02	17.20		2.68	2.72	1.22		1 10	1.24	f3 IV g8.5 IV	2.25	
589	4 18			17 22 17 13	17.17	3.71::	2.65		0.83	0.28	0.71	1.11	a8 III		6090
590 591	4 18 4 18			13 06		4.68	3.82	2.76	1.25						
592					15.78		3 7/	2.69	1 91	0.44	1.08	1.69	g6 III		3740
593					17.38		2.62:	1.94:	0.93:	0.36	0.87	1.25	f7 V a9 V		2320
594				12 10		3.57:	2.73	1.84	0.88	0.32	0.78	1.21	a9 V		3030
595	4 18			13 28	16.63		3.81:	2.71	1.22	0.45	1.09	1.71	g6 III	2.08	5470
596				16 34	17.46			1.83			0.70		+437	0.14	4100
597				17 50		3.54		1.61		0.28	0.64	1.12	a4 V a9 V		4180 3700
598				12 52	17.57			$\frac{1.78}{2.50}$	0.86 0.96	0.55	0.70	1.13	k4.5 V:	0.55	
599				29 09 15 33		4.28 3.66		1.75	0.88	0.29		1.12	11.0 11	2.00	
600 601				14 05		3.59	2.01					1.49	f9 V	1.95	2670
602			+58	16 04			2.74:	1.88:			0.75	1.20:	: a9 V		3480
603			+58	15 12	15.48		3.00	2.16	1.06	0.37			f7 III		1810
604		54.4	+58	18 05	16.64			1.77		0.32	0.71	1.14	a6 V		2890
605				17 15	15.92		2.65	1.62	0.78	0.29	0.66	1.03	a3 IV	2.28	3530
606				12 50	17.84			2.04	0.92:	0.30	0.87	1.07			
607				14 44 16 52	18.00		2.98:	2.03	0.92	0.30	0.74	1.13	a7 V	2.31	2560
608 609				13 41		3.75		1.73	0.84	0.31	0.71	1.11	a5 V-IV	2.38	2260
610				12 29		4.07	2		1.05	0.40	1.00	1.52			
611				15 22			2.75	1.79	0.85		0.73				2990
612				14 51	17.20	3.75:	2.83	1.84					a6 V		3510
613				23 58	18.11					0.36	1.02	1.56	g7 III	1.42	2000
614				15 01		3.64	2.69	1.65					a4 V-III		3690 3520
615				16 41			2.73	1.74	1.00.	0.29	0.72	1.00	a6 V-III g1.5 IV		3090
616				24 35 14 35	17.38	3.63		1.80		0.40	0.72	1.12	a8 V		2600
617 618				13 58		3.75	2.80	1.78	0.87			1.11	a5 V	2.42	3750
619		55.8		15 53		4.49		2.67	1.19	0.43	1.07	1.66	g8 III	1.75	3770
620				13 51	17.34		2.74	1.79	0.86	0.28	0.72	1.12	a9 III		6170
621				12 43	16.10	3.73	2,77	1.73	0.84	0.31	0.73	1.14	a4 V-III		2570
622	4 18			19 57	15.73	3.94		2.32	0.93	0.43	0.92	1.32	k1.5 V	1.16	
623				28 21		3.29:		1.61	0.72				f3 III		6780 3070
624				14 11		3.61		1.89	0.92				a9 V f2 III:	2.30 1.67	6100
625		56.4		09 54		3.38 3.70:		1.78	0.87		0.77		a7 V		2720
626 627		56.4 56.6		3 14 21 3 15 33	17.75	3.62:		1.71	0.82				a9 III		5720
628		56.7		03 45	17.55		2100		1.15	0.47	1.08	1.61	k0 IV	1.88	3260
629		56.7		16 01		3.66	2.69	1.70	0.80		0.63	1.01	a5 V		3640
630		56.8		13 17		3.76	2.76	1.76		0.31	0.69	1.08	a6 III	2.33	4860
631		56.9	+58	10 54	14.32	3.52:		1.61	0.85	0.26	0.72	: 1.05	b9.5 V		1620
632	4 18	56.9		3 13 02				1.78	0.87				a7 IV		5310
633		56.9		15 31				2.72	1.18				g8 III	1.85	3370 3620
634		56.9		12 47		3	2.86	1.78	0.83			1.17	: a3 V-III : a8 III		2310
635		57.1		14 44		3.74	2.72	1.76	0.86	0.32	0.77	1.10	f5 V	1.96	2670
636		57.2 57.2		3 08 36 3 04 43			2.04	2.20	1,06	0.36	0.93	1.40	19 V-III		2220
637	4 18	01.2	7-00	04 43	11.90	,		2.20	1.00	. 0.00	0.00	2.70			-

Table 3. Continued

No.	RA(2000)	DEC(2000) <i>V</i>	U-V	P-V	X-V	Y-V	′ Z-V	V-8	V-I	Photom.	A_V	d
	hm s	0 / //	mag 1	mag	nıag	mag	mag	mag	mag	mag	sp. type	mag	pc
638	4 18 57.3	+58 14 23	15.03	4 46	3.72	2.63	1.16	0.45	1.00	1 00	kOIV	1.00	1050
639	4 18 57.3	+58 13 24		4.40		2.03 : 1.95:					f4V-III		1050 3080
640		+58 13 52		3.79		1.86	0.90				fi III		3640
641	4 18 57.3	+58 16 53				1.64	0.80				a4 V-IV		2380
642	4 18 57.4	+58 12 05	17.80	3.50	2.76	: 1.98	0.95	0.34	0.84	1.29	f7 IV		4620
643	4 18 57.5	+58 22 29				: 2.78	1.24	0.49			g9 III		6020
644	4 18 57.5	+58 18 14				1.94	0.93	0.34			a9 IV		3810
645	4 18 57.5	+58 16 13				1.77	0.87	0.29			a9 III		4410
646 647	4 18 57.6 4 18 57.8	+58 24 19 +58 15 19				2.20 1.65	0.93			1.29	g9.5 IV		2750
648	4 18 57.9	+58 09 50					1.24			1.75	a3 IV	2.34	3910
649	4 18 57.9	+58 13 19					0.86				a6 V:	2 42	3740
650	4 18 58.1	+58 15 49				1.81		0.34			b8.5 V		7600
651	4 18 58.1	+58 07 13				2.65	1.22	0.40			g2.5 III		4540
652	4 18 58.2	+58 18 27	18.19 3			1.96	0.95	0.36			លេខ		3710
653	4 18 58.4	+58 19 11	16.94 3			1.67	0.81	0.31			a8 III		5880
654	4 18 58.5	+58 18 54	17.88 3			1.77	0.82	0.35			f0 V		4230
655	4 18 58.5	+58 15 46	16.29 3			1.64	0.79	0.29	0.66		a4V		3090
656 657	4 18 58.5 4 18 58.6	+58 12 00 +58 15 14	17.54 3 15.54 3		$\frac{2.72}{2.71}$	1.95	0.96	0.33			f4 IV		4130
658	4 18 58.7	+58 13 14 +58 13 57	15.26 4			$\frac{1.74}{2.62}$	$0.86 \\ 1.22$	$0.32 \\ 0.45$	1.08		a6 V	2.32	1750
659	4 18 58.8	+58 07 21	17.42			2.01	0.95	0.31			f9 V-III	1 82	1950
660	4 18 58.9	+58 11 04	18.21 3	3.50			0.93	0.36	0.79		f2 V		4240
661	4 18 58.9	+58 15 08	15.34 4	1.46	3.60	2.58	1.18	0.43	1.07	1.68			
662	4 18 59.0	+58 21 59	16.26 3			2.01	0.96	0.35	0.89	1.38	f6 IV	2.05	2120
663	4 18 59.0	+58 16 51	17.53 3	3.58:	2.89:	2.10		0.39			g1.5 V		1780
664	4 18 59.2	+58 15 55	18.10	. 0.4	4.40		0.98	0.42	0.76	1.19		2.88	
665 666	4 18 59.2 4 18 59.3	+58 17 58 +58 14 01	15.89 5 17.11 3		4.48	3.16 1.76	1.36 0.81	0.54	1.22		k1.2 III		4150
667	4 18 59.3	+58 04 27	17.81		2.10	1.68	0.84	0.29	0.67 0.65		a5 V-III: a3 V		3890 6280
668	4 18 59.4	+58 14 35	17.57 3	.58	2.65	1.82	0.85	0.27	0.77		f0 IV		4700
669	4 18 59.4	+58 17 06	17.58 3			1.86	0.89	0.34	0.81		f3 III		6130
670	4 18 59.5	+58 15 29	18.05	1	2.75:	1.89	0.95	0.33	0.76		a9 V		4080
671	4 18 59.6	+58 14 03	16.66 3			1.70					a4 V-III		3430
672	4 18 59.8	+58 07 38	16.17		2.68	1.62	0.79	0.27	0.66	1.00	a3 V-IV		3050
673 674	4 18 59.8 4 18 59.9	+58 28 05 +58 25 59	17.70 18.05			1.90:							2750
675	4 18 59.9	+58 14 12	17.89		2.70:						f7 V-III:	1.68	
676	4 18 59.9	+58 19 13	17.74 3				0.88	0.21	0.00	1.29	f0 V-III a8 V	2.22 2.27	
677	4 18 59.9	+58 14 16	16.56 3				0.99	0.39			g6 IV	1.64	
678	4 19 00.0	+58 25 34	17.43		2.81:						f6 V	2.12	
679	4 19 00.0	+58 08 39	18.20				1.02		1.04				
680	4 19 00.0	+58 10 53	17.08 3	.59	2.91		1.00	0.34	0.91		g0 IV	1.76	3190
681	4 19 00.0	+58 23 03	16.91			3.26		0.60	1.19		k1.5 III	2.20	6470
682 683	4 19 00.1	+58 29 00	17.30		3.00:	2.25:			0.83		# 1 / TT-		
684	4 19 00.2 4 19 00.2	+58 07 24 +58 14 50	16.40 17.37		2.84	1.88 2.01	$0.92 \\ 0.96$				a7 V-III	2.65	
685	4 19 00.2	+58 05 19	16.16		2.80	1.76					f7 III a3 V-IV	$\frac{1.86}{2.63}$	
686	4 19 00.2	+58 10 41	17.27 3			1.58	0.76	0.28	0.59			1.97	
687	4 19 00.3	+58 13 47	16.03 3			1.75		0.31			a7 III	2.25	
688	4 19 00.3	+58 14 18	17.05 3	.49:	2.67	1.70		0.29	0.70			2.19	
689	4 19 00.4	+58 14 45	16.26 3			1.53	0.72	0.26			a3 IV	2.09	
690	4 19 00.5	+58 15 26	15.75 3.	.65	2.65	1.63		0.29			a3 V-IV	2.31	
691	4 19 00.6	+58 10 59	18.01	~.		1.81	0.87	0.31			f3 V-III	1.84	
692 693	4 19 00.6 4 19 00.6	+58 13 06	17.60 3.		2.92:			0.32	0.75	1.16	a6 V:	2.49	
694	4 19 00.6	+58 15 59 +58 23 54	15.56 3. 18.38	.04	2.70:	1.66:					a4 V	2.28	2170
695	4 19 00.7	+58 23 54	18.38 18.31 3.	64		1.76:					f1 V-III	9.04	4100
696	4 19 00.8		16.80 3.		2.64	1.65			0.63			2.34 2.16	
697	4 19 00.8		15.18 3.		3.26						g9.5 III	0.52 -	
698	4 19 00.8	+58 12 34	16.99 3.					0.31	0.67	1.06	a5 V:	2.38	
699	4 19 01.0	+58 16 46	15.13 2.					0.25	0.52			2.50	
700	4 19 01.0	+58 24 18	17.68		2.70:			0.37	0.83		f1 V	2.24	3290
701	4 19 01.1	+58 14 40	18.02	:	2.70:	1.73	0.81	0.30	0.64	1.08	a5 V-III	2.24	6270

Table 3. Continued

тa	ible 3. C	ontinuea											
No.	RA(2000)	DEC(2000)	V	U– V	P– V	X-V	Y-V	Z– V	V– S	V-I	Photom.	A_V	d
	h m s	0 / //	mag	mag	mag	mag	mag	mag	mag	mag	sp. type	mag	рс
702	4 19 01.1	+58 05 36	14.61	4.67	3.74	2 69	1.25	0.45	1.12	1.81			
703	4 19 01.3	+58 15 11		: 3.50			0.90	0.34	0.79		f0 V	2.21	4110
704	4 19 01.3	+58 17 52	17.54		2.80:		0.91	0.30			a3 V-III	2.71	
705	4 19 01.3	+58 11 59	15.88		3.02		1.09	0.38				2.68	940
706	4 19 01.4	+58 24 14	17.03		2.75			0.38	0.81			2.26	2430
707	4 19 01.5	+58 24 02	17.26		2.60	1.64		0.28	0.69	1.06	a6 V	2.07	4350
708	4 19 01.7	+58 08 59	16.01		2.57						a3 IV	2.14	3930
709	4 19 01.7	+58 20 23	16.66	3.48	2.57	1.62	0.78	0.28	0.67	1.06	a6 V	2.03	3350
710	4 19 01.7	+58 14 33	16.61		2.72	1.70	0.86				a3 V-III	2.49	
711	4 19 02.0	+58 23 29	15.71	3.57	2.64	1.70	0.81		0.69	1.07	a6 V		2030
712	4 19 02.0	+58 19 25	17.23			1.95	0.95	0.35	0.87	1.35	f6 V a3 III		2150
713	4 19 02.1	$\pm 58 09 09$	16.28			1.62	0.81	0.28	0.71	1.06	a3 III	2.39	
714	4 19 02.1	$+58\ 15\ 21$	15.68			1.74	0.82				a6 V-IV		1880
715	4 19 02.2	+58 14 41	16.38	3.72	2.74	1.71	0.83	0.30				2.38	3020
716	4 19 02.3	+58 05 25	18.09			1.80:		0.29	0.85				
717	4 19 02.3	+58 14 29	16.22			1.66	0.80				a3 V-IV		3030
718	4 19 02.4	+58 09 16	16.81		2.61			0.31					2350
719	4, 19 02.5	+58 21 00	16.72		2.65			0.35			1917	1.80	2980
720	4 19 02.5	+58 26 11	17.29		2.97: 2.58		0.97 0.79	0.42	0.67	1.01	a5 V-IV	2.03	3740
$\frac{721}{722}$	4 19 02.5 4 19 02.5	+58 19 38 +58 29 23	16.69 17.65								al.5 V	2.06	
723	4 19 02.5	+58 15 32	14.58		2.55						a6 V	1.95	
724	4 19 02.5	+58 12 28	17.44		2.93	2 17	1.01				f9.5 V		1740
725	4 19 02.7	+58 16 07	16.33		3.34	2.42	1.13	0.41	1.05	1.63	e2.5 IV		1640
726	4 19 02.7	+58 19 41	17.93			1.77:		0.31	0.78	1.21	g2.5 IV f1 V-III		4290
727	4 19 02.9	+58 06 54	14.70		2.79		0.95	0.35	0.88	1.34	f3 V	2.23	
728	4 19 02.9	+58 18 32	17.99		2.74:		0.93		0.88				2760
729	4 19 02.9	+58 08 48	18.40			1.91:					f9.5 V-III		
730	4 19 03.0	+58 16 28	15.71		3.76		1.22				g6 III		3560
731	4 19 03.0	+58 09 15	17.38			1.80	0.89	0.28	0.90	1.36	f2 V-III	2.04	2930
732	4 19 03.0	+58 09 18	16.62	3.37	2.70	1.88					g0 IV		3060
733	4 19 03.3	+58 14 04	16.40	3.80	2.74	1.80		0.30					3710
734	4 19 03.3	+58 16 19	15.66		3.74		1.20	0.44	1.08	1.70	g9.5 IV		1320
735	4 19 03.3	$+58\ 10\ 45$		3.37:	2.57						a1.5 V-III:	2.23	5650
736	4 19 03.4	+58 29 28		3.70:	3.03:		0.97		0.80				
737	4 19 03.4	+58 03 56	17.55			1.97					f2 V-III:	2.47	2600
738	4 19 03.4	+58 08 55	17.91		2.45:		0.81		0.83				-050
739	4 19 03.4	+58 14 07	16.81		2.69		0.81				a8 III		5270
740	4 19 03.6	+58 12 51	15.64		2.93		0.92	0.37			g8 V		620 4020
741	4 19 03.7	+58 14 28		3.61:		1.76	0.87				a7 V-IV a6 V-IV		2060
742 743	4 19 03.8	+58 15 48	15.99		2.77 2.73:	1.78	$0.86 \\ 0.92$				fi V-III		3510
744	4 19 03.8 4 19 03.9	+58 12 59 +58 26 17	17.81 17.31		2.72:			0.34					2080
745	4 19 03.9	+58 24 38	18.03								a9 V-III		4050
746	4 19 03.9	+58 18 49	15.62		2.56						a3 IV		3280
747	4 19 04.0	+58 15 09	16.85		2.75			0.30					3480
748	4 19 04.0	+58 05 03	18.15		2.10		1.00		1.01				2340
749	4 19 04.2	+58 13 20	17.66		2.81:		1.01				f5 IV		4040
750	4 19 04.2	+58 09 20	17.41		2.76		0.83				a6 V-III		4070
751	4 19 04.3	+58 17 27	16.94		2.72		0.85		0.71				3350
752	4 19 04.3	+58 08 24	18.26		-	1.78:		0.28			f9 V-IV		3830
753	4 19 04.3	+58 10 48	14.93		3.21		0.94	0.41			k1.2 V	1.00	354
754	4 19 04.3	+58 15 20	16.02		2.74		0.82				a3 IV	2.42	3470
755	4 19 04.4	+58 22 52	17.30		2.72	1.87	0.91				f3 III		5300
756	4 19 04.4	+58 14 31	15.65	4.60	3.82		1.23				g8 III		3940
757	4 19 04.4	+58 14 00	15.65		2.73						a5 V-IV		1990
758	4 19 04.4	+58 17 41			3.16:						g4 IV	1.83	3410
759	4 19 04.5	+58 15 50	17.09		2.74						a6 V-III	2.35	3540
760	4 19 04.5	+58 16 46	17.39	3.58:			0.90	0.38	0.73	1.21	a9 V	2.33	3110
761	4 19 04.6	+58 13 02	17.06		3.52:						g5 III		7230
762	4 19 04.6	$+58\ 25\ 56$	18.08								g7 V		2440
763	4 19 04.7	$+58\ 15\ 17$	18.00		2.74:						a7 V-III		4810
764	4 19 04.7	+58 04 47	17.22			2.12	1.02	0.36	0.91	1.40	f7 V		1790
765	4 19 04.8	+58 13 42	16.25	3.74	2.74	1.74	0.86	0.31	0.75	1.17	a5 V-III	2.40	2570

Table 3. Continued

No.	Table 3. (Continued										
Total Tota	No. BA(2000)	DEC(2000)	V U	-V P-V	X-V	Y-V	Z– V	V– S	V– I	Photom.	A_V	d
767 4 19 05.0 + 581 64 8 15.97 3.72 2.73 1.70 0.82 0.29 0.71 1.12 1.78 g.9.51V 2.45 2710 769 4 19 05.0 + 581 64 10 15.89 3.79 2.79 1.76 0.82 0.29 0.71 1.12 1.78 g.9.51V 2.45 2710 777 4 19 05.0 + 581 40 11 5.89 3.79 2.79 1.76 0.82 0.29 0.71 1.12 1.78 g.9.51V 2.45 2710 777 4 19 05.1 + 580 24 10 17.31 3.42: 2.70 1.90 0.89 0.33 0.84 1.25 g01V 1.40 4180 777 4 19 05.2 + 581 19 05 16.94 3.40 2.60 1.66 0.79 0.30 0.66 1.06 41V 2.22 40 777 4 19 05.2 + 585 19 76 16.17 3.72 2.73 1.73 0.82 0.30 0.71 1.08 a5.7 5 2.33 2.50 1.77 4 19 05.5 + 585 20 40 18.14 7.77 4 19 05.5 + 585 20 40 18.14 7.77 94 19 05.5 + 585 20 16 17.84 1.77 1.78 4 19 05.5 + 585 19 17 17.08 4.67 1.77 1.78 1.78 1.78 1.78 1.78 1.78 1.7			mag m	ag mag	mag	mag	mag	mag	mag	sp. type	mag	рс
767 4 19 05.0 + 581 64 8 15.97 3.72 2.73 1.70 0.82 0.29 0.71 1.12 1.78 g.9.51V 2.45 2710 769 4 19 05.0 + 581 64 10 15.89 3.79 2.79 1.76 0.82 0.29 0.71 1.12 1.78 g.9.51V 2.45 2710 777 4 19 05.0 + 581 40 11 5.89 3.79 2.79 1.76 0.82 0.29 0.71 1.12 1.78 g.9.51V 2.45 2710 777 4 19 05.1 + 580 24 10 17.31 3.42: 2.70 1.90 0.89 0.33 0.84 1.25 g01V 1.40 4180 777 4 19 05.2 + 581 19 05 16.94 3.40 2.60 1.66 0.79 0.30 0.66 1.06 41V 2.22 40 777 4 19 05.2 + 585 19 76 16.17 3.72 2.73 1.73 0.82 0.30 0.71 1.08 a5.7 5 2.33 2.50 1.77 4 19 05.5 + 585 20 40 18.14 7.77 4 19 05.5 + 585 20 40 18.14 7.77 94 19 05.5 + 585 20 16 17.84 1.77 1.78 4 19 05.5 + 585 19 17 17.08 4.67 1.77 1.78 1.78 1.78 1.78 1.78 1.78 1.7	700 4 10 04 0	J-58 20 05	18.05.4	06	2.47.	1.06	0.47	1.02	1.53	k1.2 V	1.55	1150
768 4 10 65.6 15.8 16 14.18.7 2.59 2.70 1.0 0.82 0.29 0.71 1.1 2 dV-11 2.49 2.99 1.70 0.82 0.30 0.70 1.11 4 V-IV 2.49 2.99 777 4 19 0.51 +58 21 17.3 3.42 2.70 1.06 0.89 0.30 0.66 1.06 at V-IV 2.24 40 773 4 19 0.62 +58 13 71 4 2.06 0.60 0.79 0.30 0.66 1.06 at V-IV 2.22 40 776 4 19 0.64 +58 17 1.10 4.5 2.64 1.08 0.79 0.30 0.71 1.08 38 1.09 3.29 2.73 1.07 0.80 3.97 1.00 3.00 0.01 1.08 3.97 1.00 3.00 0.01 1.08 3.97 1.00 <td< td=""><td></td><td></td><td></td><td>.00</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>				.00								
777 4 19 05.0 +58 14 01 15.89 3.79 2.79 1.76 0.84 0.30 0.70 1.11 44V-IV 2.49 2290 771 4 19 05.1 +58 20 17 13.342; 2.70 1.90 0.89 0.33 0.34 1.25 g0IV 1.40 4180 772 4 19 05.1 +58 20 37 16.35 3.62 2.65 1.63 0.78 0.30 0.66 1.06 44IV 2.22 4040 773 4 19 05.2 +58 11 37 16.17 3.72 2.73 1.73 0.82 0.30 0.61 1.02 8V 1.93 3320 774 4 19 05.2 +58 0.54 16.19 3.72 2.74 1.73 0.82 0.30 0.71 1.08 85 V 2.34 2540 775 4 19 05.5 +58 20 40 18.14 2.82; 181 0.88 0.29 0.78 1.10 1.08 85 V 2.33 120 1776 4 19 05.5 +58 20 40 18.14 2.82; 181 0.88 0.29 0.83 1.29 87 V-III 2.33 1420 1778 4 19 05.5 +58 20 40 18.14 2.82; 181 0.88 0.29 0.83 1.29 87 V-III 2.54 54810 778 4 19 05.5 +58 20 34 17.14 3.55 2.26 1.30 0.49 1.14 1.89 g3 III 2.73 4740 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.0		+58 16 48	15.97 3.							a4 V-IV	2.39	2490
777 4 19 05.1 +58 24 10 17.31 3.42: 2.70 1.90 0.89 0.33 0.84 1.25 g0 IV 1.40 4180 772 4 19 05.1 +58 20 37 16.35 3.22 2.65 1.68 0.78 0.30 0.66 1.06 al V 2.22 4040 773 4 19 05.2 +58 11 37 16.17 3.72 2.73 17.3 0.82 0.30 0.66 1.06 al V 2.22 4040 774 4 19 05.2 +58 0.85 54 16.19 3.02 2.66 1.66 0.79 0.30 0.66 1.02 a8 V 1.96 3320 777 4 19 05.5 +58 20 40 18.14 23 2.41 1.11 0.45 1.02 1.60 g.5 V. 1.98 1040 778 4 19 05.5 +58 20 40 18.14 27 17.08 4.67 3.78 1.28 1.28 1.28 1.28 1.28 1.28 1.28 1.2										+437 BV	9.40	2200
777 4 19 05.2 +58 10 37 16.35 3.62 2.66 1.63 0.78 0.30 0.66 1.06 4 IV 2.22 4040 777 4 19 05.2 +58 11 37 16.17 3.72 2.73 1.73 0.82 0.30 0.71 1.08 85 V 2.34 2540 777 4 19 05.5 +58 0.5 14 16.19 3.22 2.64 1.82 0.78 0.72 0.70 1.06 85 V 2.33 120 1776 4 19 05.4 +58 17 46 17.65 4.23 2.42 1.11 0.45 1.02 1.60 85 V 1.23 120 1777 4 19 05.5 +58 0.9 0 18.14 2.82 1.11 0.85 0.0 0.83 1.29 97 V-III 2.73 4740 779 4 19 05.7 +58 18 51 17.14 3.50 2.5 2.65 1.06 0.78 0.33 0.64 1.01 86 V 2.08 4457 778 4 19 05.7 +58 0.9 16 17.84 2.25 1.11 0.85 0.0 0.29 0.83 1.29 97 V-III 2.73 4740 779 4 19 05.7 +58 0.81 25 17.14 3.50 2.26 1.76 0.84 0.33 0.41 1.01 86 V 2.08 4457 84 19 05.5 +58 20 26 15.09 4.45 3.75 2.66 1.77 0.83 0.29 0.73 1.16 81 V 2.09 4910 78.8 4 19 06.1 +58 06 17 17.73 2.52 2.50 1.06 0.77 0.83 0.29 0.73 1.16 81 V 2.09 4910 78.8 4 19 06.6 +58 13 22 16.15 3.72 2.58 1.74 0.95 0.33 0.96 1.47 (711 1.18 3.15 2.78 1.18 0.18 0.18 0.18 0.18 0.18 0.18 0.1												
773 4 19 06.2 +58 19 05 16.94 3.40												
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777 4 19 0.5. + 58 20 40 18.14 778 4 19 0.5. + 58 20 40 18.14 779 4 19 0.5. + 58 18 51 17.32 3.52 780 4 19 0.5. + 58 18 51 17.32 3.52 781 4 19 0.5. + 58 18 51 17.32 3.52 781 4 19 0.5. + 58 18 51 17.32 3.52 782 4 19 0.5. + 58 18 52 17.54 3.57 782 4 19 0.5. + 58 18 52 17.54 3.57 783 4 19 0.5. + 58 18 52 26 15.09 4.45 784 4 19 0.5. + 58 18 22 26 15.09 4.45 785 4 19 0.6. + 58 18 25 26 17.07 3.92: 786 4 19 0.6. + 58 13 22 16.15 3.78 787 4 19 0.5. + 58 13 22 16.15 3.78 789 4 19 0.5. + 58 13 22 16.15 3.78 789 4 19 0.5. + 58 13 22 16.15 3.78 789 4 19 0.5. + 58 13 22 16.15 3.72 789 4 19 0.5. + 58 13 22 16.15 3.72 790 4 19 0.5. + 58 13 21 15.59 3.72 791 4 19 0.5. + 58 13 21 15.59 3.72 793 4 19 0.6. + 58 13 21 15.59 3.72 794 4 19 0.6. + 58 13 21 15.59 3.72 794 4 19 0.6. + 58 13 22 16.15 3.84 795 4 19 0.6. + 58 13 22 16.15 3.84 796 4 19 0.7. + 58 15 10 18.05 797 4 19 0.8. + 58 15 17 16.33 3.63 793 4 19 0.8. + 58 15 17 16.33 3.63 794 4 19 0.7. + 58 15 10 18.05 797 4 19 0.8. + 58 15 10 18.05 798 4 19 0.8. + 58 15 12 18.05 799 4 19 0.8. + 58 15 12 18.05 797 4 19 0.8. + 58 15 12 18.05 798 4 19 0.8. + 58 15 12 18.05 799 4 19 0.8. + 58 15 12 18.05 799 4 19 0.8. + 58 15 12 18.05 799 4 19 0.8. + 58 15 12 18.05 790 4 19 0.8. + 58 15 12 18.05 791 4 19 0.8. + 58 15 17 16.33 3.77 791 4 19 0.7. + 58 15 22 11 4.42 3.5 801 4 19 0.7. + 58 15 17 16.33 3.77 799 4 19 0.8. + 58 22 11 14.42 3.5 801 4 19 0.7. + 58 17 25 16.33 3.77 801 4 19 0.7. + 58 17 25 16.33 3.77 801 4 19 0.7. + 58 17 25 16.33 3.77 801 4 19 0.7. + 58 17 25 16.33 3.77 802 4 19 0.8. + 58 22 21 18.34 3.84 803 4 19 0.7. + 58 17 25 16.33 3.84 803 4 19 0.7. + 58 17 25 16.33 3.84 803 4 19 0.7. + 58 18 17 18.37 2.83 801 4 19 0.8. + 58 22 11 14.23 3.85 801 4 19 0.8. + 58 22 11 14.23 3.85 801 4 19 0.8. + 58 22 11 14.23 3.85 801 4 19 0.8. + 58 22 11 14.23 3.85 801 4 19 0.8. + 58 22 11 14.23 3.85 801 4 19 0.8. + 58 22 11 14.23 3.85 801 4 19 0.8. + 58 20 10 18.52 802 4 19 0.8. + 58 20 10 18.52 803 4 19 0.8. + 58 20 10 18.52 804 4 19 0.8. + 58 20 10 18.52 805 4 19 0.8. + 58 20 10 18.52 80												
778 4 19 0 6.6 -58 11 27 17 0.08 4.67 3.78:: 2.86 1.31 0.49 1.14 1.89 g3 III 2.73 4740 779 4 19 0 5.7 -58 00 9 16 17.34 3.50 2.66 1.67 0.33 0.71 1.07 a 5 V.III 2.08 4450 781 4 19 0 5.7 -58 00 9 34 17.14 3.50: 2.66 1.77 0.84 0.33 0.71 1.07 a 5 V.III 2.40 5330 783 4 19 0 5.9 +58 29 26 15.09 4.45 3.72 2.66 1.77 0.83 0.29 0.85 1.57 kl.7V: 1.83 244 784 4 19 0 6.1 +58 10 55 17.53 3.72 2.66 1.77 0.85 0.29 0.81 1.42 [21 V.III 1.83 244 787 4 19 0 6.1 +58 13 56 16.15 3.72 2.73 1.74 0.86 0.31 0.44 1.11 a 81II 2.21 3640 788 4 19 0 6.5 +58 13 51 15.75 2.58 1.78 0.85 0.93 1.41 1.91 2.11 2.11 2.23 2.04												
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785 4 19 06.1 +58 06 17 17.73 2.58: 1.78 0.85 0.29 0.81 1.22 1.22 13640 787 4 19 06.2 +58 13 22 16.15 3.78 2.76 1.78 0.84 0.27 0.75 1.14 a8 III 2.21 3640 788 4 19 06.5 +58 13 25 16.15 3.78 2.73 1.74 0.86 0.31 0.74 1.19 a5V-IV 2.38 2470 790 4 19 06.5 +58 18 46 16.04 3.49 2.54 1.52 0.72 0.27 0.63 0.94 1.44 (9.51V 2.02 2450 790 4 19 06.5 +58 13 45 16.56 16.30 3.63 2.68 1.66 0.81 0.29 0.68 1.04 a4V-IV 2.29 3030 792 4 19 06.5 +58 13 55 17.51 1.80 5 1.42 0.63 0.81 0.23 0.95 a1V 2.08 4100 792 4 19 06.6 +58 13 25 17.89 2.72 0.70 1.65 0.81 0.25 0.69; 1.07 a3IV 2.23 230 793 4 19 06.7 +58 15 05 1 18.05 2.75; 1.87 0.91 0.32 0.77 1.15 a8V 2.31 4110 795 4 19 06.8 +58 19 58 17.38 1.38 2.1 2.75; 1.87 0.91 0.91 0.32 0.78 1.25 a9V-III 2.36 4170 796 4 19 06.7 +58 13 25 17.49 2.68 1.80 0.82 0.20 0.77 0.35 0.77 1.17 28V 2.31 4110 </td <td></td>												
Table Tabl			17.07 3.									
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814 4 19 07.8 +58 15 46 15.95 3.70 2.73 1.71 0.79 0.44: 0.55: 1.03 a4 V: 1.05: f9 V-III 2.36 2500 815 4 19 07.8 +58 03 10 17.90 2.02: 0.97 0.33 0.96 1.56: f9 V-III 1.89 2360 816 4 19 07.8 +58 13 33 18.38 3.67 2.67: 1.72: 0.91: 0.41: 0.78: 1.18 1.86 V 2.26 3100 818 4 19 08.0 +58 27 21 13.71 3.59 2.63 1.78 0.87 0.33 0.76 1.17 63II 1.73 1100 1.73 1100 820 4 19 08.2 +58 22 22 17.33 2.65 1.89 0.90 0.35 0.82 1.27 f8IV 1.56 3700 821 4 19 08.4 +58 18 09 13.12 3.25 2.69 1.68 0.80 0.31 0.75 1.14 k1.2 V: 0.16 2730 2.58 5130 823 4 19 08.4 +58 12 19 17.09 4.05 3.41: 2.42 1.08 0.42 0.99 1.47 g8IV 1.66 2920 825 4 19 08.6 +58 14 06 16.84 3.65 2.76 1.80 0.88 0.32 0.78 1.23 f2III 1.85 5980 826 4 19 08.7 +58 26 10 18.27: 419 08.8 +58 0.01 17.22 2.86: 2.03 0.92: 0.32 0.93 1.39 g5V-III 1.46 1420										19 V	1.59	3130
815 4 19 07.8 +58 03 10 17.90 2.02 0.97 0.33 0.96 1.50: f9 V-III 1.89 2360 816 4 19 07.8 +58 29 26 17.84 2.67: 1.72: 0.91: 0.41: 0.78: 1.18 2.26 3100 818 4 19 08.0 +58 27 21 13.71 3.59 2.63 1.78 0.87: 0.33 0.76: 1.17 63 III 1.73 1100 820 4 19 08.2 +58 22 21 17.33 2.65: 1.89: 0.90: 0.35: 0.82: 1.27 f8 IV 1.56: 3700 2.76: 1.69: 0.83: 0.32: 0.65: 1.10: a2V 2.58: 5130 821 4 19 08.2 +58 03 54: 16.68 2.04: 1.32: 0.48: 1.20: 1.93: g7 III 2.51: 4640 822 4 19 08.4 +58 12 19: 17:09: 4.05 3.41: 2.42: 1.08: 0.42: 0.99: 1.47 g8 IV 0.16: 2730 824 4 19 08.6 +58: 14: 06: 16.84: 3.65 2.76: 1.79: 0.84: 0.31: 0.75: 1.14: k1.2V: 0.16: 2730 0.77: 740 825 4 19 08.6 +58: 15: 35: 17: 44: 3.63 2.67: 1.80: 0.80: 0.32: 0.82: 0.78: 1.23: f2 III 1.85: 5980 827 4 19 08.7 +58: 26: 10: 18: 27: 2.25: 0.90: 0.32: 0.93: 0.32: 0.93: 1.32: f3 V-III 1.85: 0.90: 0.33: 0.83: 0.83: 1.32: f3 V-III 1.98: 2.63 1.85:										a4 V:	2.36	2500
817 4 19 07.9 +58 13 33 18.38 3.67 2.09: 1.04 0.37: 1.00: 1.48 f6 V 2.26 3100 818 4 19 08.0 +58 27 21 13.71 3.59 2.63 1.78 0.87 0.33 0.76 1.17 63 III 1.73 1100 819 4 19 08.0 +58 22 22 17.33 2.65 1.89 0.90 0.35 0.82 1.27 f8 IV 1.56 3700 820 4 19 08.2 +58 03 54 16.68 2.94 1.32 0.48 1.20 1.93 g7 III 2.51 4640 822 4 19 08.4 +58 18 09 13.12 3.25 2.69 1.86 0.80 0.31 0.75 1.05 g5 IV 0.77 740 823 4 19 08.5 +58 12 19 17.09 4.05 3.41: 2.42 1.08 0.42 0.99 1.47 g8 IV 0.66 2920 825 4 19 08.6 +58 14 06 16.84 3.65 2.76 1.70 0.84 0.31 0.72 1.14 a7 V 2.32 2910 826 4 19 08.7 +58 26 10 18.27: 2.69 1.86 0.90 0.33 0.32 0.78 1.23 f2 III 1.85 5980 0.90 0.33 0.92 0.93 1.39 g5 V-III 1.66 2920					2.02:	0.97	0.33	0.96	1.50:			
818 4 19 08.0 +58 27 21 13.71 3.59 2.63 1.78 0.87 0.33 0.76 1.17 f3 III 1.73 1100 819 4 19 08.0 +58 23 31 17.10 3.33 2.65 1.89 0.90 0.35 0.82 1.27 f8 IV 1.56 3700 820 4 19 08.2 +58 22 22 17.33 2.76 1.69 0.83 0.32 0.65 1.10 a2V 2.58 5130 2.58 5130 821 4 19 08.4 +58 29 10 18.52: 2.94 1.32 0.48 1.20 1.93 g7 III 2.51 4640 822 4 19 08.4 +58 18 09 13.12 3.25 2.69 1.86 0.80 0.31 0.75 1.05 g5 IV 0.77 740 824 4 19 08.5 +58 12 19 17.09 4.05 3.41: 2.42 1.08 0.42 0.99 1.47 g8 IV 1.66 2920 825 4 19 08.6 +58 15 35 17.44 3.63 2.67 1.80 0.88 0.32 0.78 1.23 f2 III 1.85 5980 827 4 19 08.7 +58 26 10 18.27: 1.85: 0.90: 0.33: 0.83: 1.32: f3 V-III 1.85 5980 828 4 19 08.8 +58 06 01 17.22 2.86: 2.03 0.92: 0.32 0.93 1.39 g5 V-III 1.46 1420	816 4 19 07.8	+58 29 26										
819 4 19 08.0 +58 23 31 17.10 3.33: 2.65 1.89 0.90 0.35 0.82 1.27 f8 IV 1.56 3700 820 4 19 08.2 +58 22 22 17.33 2.76 1.69 0.83 0.32 0.65 1.10 a2V 2.58 5130 821 4 19 08.2 +58 03 54 16.68 2.94 1.32 0.48 1.20 1.93 g7 III 2.51 4640 822 4 19 08.4 +58 18 09 13.12 3.25 2.69 1.86 0.80 0.31 0.75 1.05 g5 IV 0.77 740 824 4 19 08.5 +58 12 19 17.09 4.05 3.41: 2.42 1.08 0.42 0.99 1.47 g8 IV 1.66 2920 825 4 19 08.6 +58 15 35 17.44 3.63 2.67 1.80 0.88 0.32 0.78 1.23 f2 III 1.85 980 827 4 19 08.7 +58 26 10 18.27: 18.27: 828 4 19 08.8 +58 06 01 17.22 2.86: 2.03 0.92: 0.32 0.93 1.39 g5 V-III 1.46 1420												
820 4 19 08.2 +58 22 22 17.33 2.76 1.69 0.83 0.32 0.65 1.10 a2 V 2.58 5130 821 4 19 08.2 +58 03 54 16.68 2.94 1.32 0.48 1.20 1.93 g7 III 2.51 4640 822 4 19 08.4 +58 18 09 13.12 3.25 1.81: 0.74: 0.41: 0.75: 1.14 k1.2 V: 0.16 2730 823 4 19 08.5 +58 18 09 13.12 3.25 2.69 1.86 0.80 0.31 0.75: 1.05 g5 IV 0.77 740 824 4 19 08.6 +58 14 06 16.84 3.65 2.76 1.79 0.84 0.31 0.72: 1.44 av 2.32 2910 825 4 19 08.6 +58 15 35 17.44 3.63 2.67 1.80 0.80 0.31 0.72: 1.14 av 2.32 2910 826 4 19 08.7 +58 26 10 18.27: 1.85: 0.90: 0.33: 0.83: 1.32: f3 V-III 1.85 5980 827 4 19 08.8 +58 06 01 17.22 2.86: 2.03 <td></td>												
821 4 19 08.2 +58 03 54 16.68 2.94 1.32 0.48 1.20 1.93 g7 III 2.51 4640 822 4 19 08.4 +58 18 09 13.12 3.25 2.69 1.86 0.80 0.31 0.75 1.14 k1.2 V: 0.16 2730 824 4 19 08.5 +58 12 19 17.09 4.05 3.41; 2.42 1.08 0.42 0.99 1.47 g8 IV 1.66 2920 825 4 19 08.6 +58 14 06 16.84 3.65 2.76 1.70 0.84 0.31 0.72 1.14 a7 V 2.32 2910 826 4 19 08.7 +58 26 10 18.27; 1.85 0.90; 0.33; 0.32; 1.32; f3 V-III 1.85 5980 827 4 19 08.8 +58 50 601 17.22 2.86; 2.03 0.92; 0.32 0.93 1.39 g5 V-III 1.46 1420												
823 4 19 0.8.4 +58 18 0.9 13.12 3.25 2.69 1.86 0.80 0.31 0.75 1.05 g5 IV 0.77 740 824 4 19 0.8.5 +58 12 19 17.09 4.05 3.41: 2.42 1.08 0.42 0.99 1.47 g8 IV 1.66 2920 825 4 19 0.8.6 +58 15 35 17.44 3.63 2.67 1.80 0.84 0.31 0.72 1.14 aV 2.32 2910 826 4 19 0.8.6 +58 15 35 17.44 3.63 2.67 1.80 0.88 0.32 0.78 1.23 f2 III 1.85 5980 827 4 19 0.8.8 +58 0.00 17.22 2.86 2.03 0.92 0.32 0.93 1.39 g5 V-III 1.46 1420	821 4 19 08.2	+58 03 54	16.68		2.94	1.32	0.48	1.20	1.93	g7 III	2.51	4640
824 4 19 08.5 +58 12 19 17.09 4.05 3.41: 2.42 1.08 0.42 0.99 1.47 g8 IV 1.66 2920 825 4 19 08.6 +58 14 06 16.84 3.65 2.76 1.79 0.84 0.31 0.72 1.14 a7 V 2.32 2910 826 4 19 08.6 +58 15 35 17.44 3.63 2.67 1.80 0.88 0.32 0.78 1.23 f2 III 1.85 5980 827 4 19 08.7 +58 26 10 18.27: 1.85 0.90: 0.33: 0.33: 1.32: f3 V-III 1.95 4270 828 4 19 08.8 +58 06 01 17.22 2.86: 2.03 0.92: 0.32 0.93 1.39 g5 V-III 1.46 1420												
825 4 19 08.6 +58 14 06 16.84 3.65 2.76 1.79 0.84 0.31 0.72 1.14 a7V 2.32 2910 826 4 19 08.6 +58 15 35 17.44 3.63 2.67 1.80 0.88 0.32 0.78 1.23 f2 III 1.85 5980 1.85 4 19 08.7 +58 26 10 18.27: 1.85 0.90: 0.33: 0.83: 1.32: f3 V-III 1.95 4270 828 4 19 08.8 +58 06 01 17.22 2.86: 2.03 0.92: 0.32 0.93 1.39 g5 V-III 1.46 1420												
826 4 19 08.6 +58 15 35 17.44 3.63 2.67 1.80 0.88 0.32 0.78 1.23 f2 III 1.85 5980 827 4 19 08.7 +58 26 10 18.27: 1.85: 0.90: 0.33: 0.83: 1.32: f3 V-III 1.95 4270 828 4 19 08.8 +58 06 01 17.22 2.86: 2.03 0.92: 0.32 0.93 1.39 g5 V-III 1.46 1420												
827 4 19 08.7 +58 26 10 18.27: 1.85: 0.90: 0.33: 0.83: 1.32: f3 V-III 1.95 4270 828 4 19 08.8 +58 06 01 17.22 2.86: 2.03 0.92: 0.32 0.93 1.39 g5 V-III 1.46 1420												
	827 4 19 08.7	+58 26 10	18.27:		1.85:	0.90:	0.33:	0.83:	1.32:	f3 V-III	1.95	4270
829 4 19 09.1 +58 09 39 16.59 3.66 2.64 1.65 0.80 0.28 0.72 1.09 a5 V-III 2.22 3260												
	829 4 19 09.1	+58 09 39	16.59 3.	00 2.04	1.05	บ.ชบ	0.28	0.72	1.09	ao v-III	2.22	526U

Table 3. Continued

Ta	ipie 3. (Jontini	iea											
No	RA(2000)	DEC(2	000)	\overline{V}	U-V							Photom.	A_V	d
110.	hm s	0 /	11	mag	mag	mag	mag	mag	mag	mag	mag	sp. type	mag	\mathbf{pc}
		. =0 .		10 10	0.00	2.71	1.72	0.82	0.30	0.68	1 07	a5 V	2.28	2940
830	4 19 09.2	+58 14 +58 12	1 14	10.42	3.00	2.71		1.02:						
831 832	4 19 09.2 4 19 09.2	+58 13		16.08	4.68	3.83		1 05	0.44	1 10	1 76			
833	4 19 09.2	+58 13				0.00	1.96	0.95	0.30	0.87	1.30	f2 V	2.28	3450
834	4 19 09.3	+58 00		17.83			2.17:	0.96	0.32	0.94	1.38:	g2.5 III	1.40	
835	4 19 09.5	+58 17	7 21	16.79		2.89		0.98	0.36	0.90	1.38	f9.5 IV	1.82	
836	4 19 09.5	+58 13		16.92		2.70		0.82	0.31	0.65	1.03	a5 V	$\frac{2.22}{2.16}$	
837	4 19 09.6	+58 10		16.80		2.67		0.80	0.30	0.65	1.03	a5 V a7 V-IV	2.10	#19D
838	4 19 09.6	+58 23				2.57		0.82	0.29	0.70	1.12	27 V-1 V	2.04	2440
839	4 19 09.7	+58 1		17.81		2.77:		0.83		0.92	1.09	f7 V a3 III	2.51	3920
840	4 19 09.7	+58 14		15.87 17.97		2.73	2.09	0.99		0.88	1.39		2.08	
841	4 19 09.7	+58 21 +58 19		17.57		2.94:		0.97	0.36	0.93	1.36	g3 V	1.73	1670
842 843		+58 1	5 10 5 N7	17.15		2.82		0.84	0.32	0.67	1.09	a4 V-III	2.40	4260
844		+58 0		16.06		2.67	1.71	0.85	0.28	0.78	1.15	a7 V-III		2070
845		+58 1			3,65	2.64	1.58	0.78	0.20	0.67	1.02	a3 V-III	2.28	3630
846		+58 10	6 17		3.72	2.78	1.76	0.82	0.30	0.67	1.06	a5 V f2 V-III		3590
847	4 19 10.2	+58 0	3 31	17.50		_		0.92	0.31	0.87	1.39	12 V-III	2.16	2940
848						4.19	3.04	1.34	0.48	1.19	1.91	59 III	1 08	4760
849		+58 1			3.63	2.01	2.50	1 16.	0.30	1 06.	1.72	a8 III g8 IV	2.06	3650
850				17.98 18.37			2.00.	0.97	0.33	0.92	1.33	f9 V-III	1.79	3060
851 852		+58 1	1 50		2.75	2.80:	1 03	0.91	0.31	0.79	1.20	f3 III	1.98	6270
853				17.63		2.62	1.68	0.78	0.27	0.72	1.06	a7 V-III	2.13	4580
854				18.11		2.85:	2.03:	0.83:	0.30	0.95	1.40	g2.5 III	1.09	
855			5 19	15.11	3.84	2.78	1.76	0.86	0.31	0.76	1.20	a4 IV	2,54	1960
856		+581	8 23	17.67	,	2.68:	1.80	0.89	0.32	0.73	1.13	a9 V-IV	2.21	3740
857				18.05	i:		2.27:	1.05	0.40:	0.94	1.47	: g4 V-III	7.93	4010
858				17.45	3.74	2.80	2.28	1.08	0.31	0.72	1.13	a6 V g4 V	1.98	1570
859				17.82	ee.		1.05	0.03	0.44	0.53	1.37	: f2 V-III:	2.27	4420
860 861				18.49	3.66: 3.49 3.53 3.41		2.03	0.95	0.34	0.92	1.36	g0 V	1.72	3100
862				17.96	3 5 3		1.81	0.86	0.27	Λ 70	1 17	• fn \$/_fff	2 15	4170
863				18.28	3.41		1.93	0.93	0.33	0.88	1.35	f9 V f2 IV a9 V-IV:	1.63	3160
864				17.41	3.56	2.71	1.88	0.92	0.31	0.84	1.27	f2 IV	2.09	4020
865		+58 1	3 37		3.62	2.87:	: 1.87	0.92	0.33	0.79	1.26	a9 V-IV:	2.37	4170
866			5 18	17.95		2.71:	1.90:	0.97:	0.42	0.78	1.23	17.03	2.00	2930
867		+58 1	5 54	17.59)	2.69	1.92	0.95 0.83	0.31	0.80	1.00	f3 V a5 V-III:	2.32	4330
868		+58 1	6 44	17.30	3.54:	2.75	1.73	0.03	0.30	0.87	1.38	40 4-111.	2.02	1000
869				17.88	3.70		1.62	0.75		0.71	0.99	f9 V-III	0.88	3710
870 871				15.98		3.87	2.76	1.25					2.26	3680
872		+58 1	0 01	16.68	4.11		2.49		0.47	1.04	1.56	6 g6 III 6 k0.7 V 9 g7 IV	1.67	
873		+58 0	7 20	15.5	2 3.54	2.97	2.07	0.87	0.35	0.88	1.29	g7 IV	1.01	1940
874	4 19 11.6	+58 0	8 13	18.0		2.63	1.64			0.69	0.92	: : 1.0 0 W	1.40	770
875								1.04				k3.2 V	1.40	110
876							1.76 1.92	0.83		0.81	1.20) f3V:	2.13	1750
877		+58 2	(† 12 M 50		3.57 1 3.65		1.63	0.94		0.68	1.02	a3 V-III	-2.35	3720
878			14 09 24 57	16.0	2 3.69:	2.79	1.73							
879 880					9 3.54	2.63	1.78	0.88	0.34	0.79	1.21	f3 III	1.74	7870
881				17.7			1.84	0.88	0.32	0.74	1.12	7 a5 V 1 f3 III 2 a8 V 3 k3 V 3 g3 V 3 f9 V 1 a0 V 0 a4 V-III	2.35	3950
882					4 4.15	3.56	2.49	0.99	0.49	0.96	1.18	3 k3 V	1.11	610
883	3 4 19 12.2	+58 1	19 03	16.9	4 3.44		2.02	0.91		0.85	1.26	3 g3 V	1.40	1450
884	4 4 19 12.2						2.11	0.99		0.97	1.48	19 V	1.95	7 5570
885						2.75				0.72	1.1	1 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.31	3000
886					0 3.76		1.74			. 0.09 19.0	1.10	6 f1 V	1.98	3 1590
887					4 3.39	2.57 2.72				n or	1 1 22	2 folls	2.02	7 3200
888					9 3.71 1 4.45	3.68				1.06	1.6	5 g6 III	1.92	3200
889 890				16.9	_ ~.~	0.00	2.92	1.26		1.15	1.70	6 g9.5 III	2.00	
891				17.4	$\hat{9}$	2.72	1.90	0.94	0.34	0.81	1.28	8 f2 IV	2.12	2 4120
892		3 4-58 (n 7 57	17.9	3		1.81	0.84	0.30	0.82	1.14	6 g9.5111 8 f2 IV 4 f9 V-III 7 f2 V	1.33	3 3090
893			10 40	18.1	7 3.56		1.89	: 0.95	0.32	0.84	1.3	7 f2 V	2.1	7 3970

Table 3. Continued

	inie 9'			_		_					
No.	RA(2000)	DEC(2000)								A_V	d
	hm s	0 / //	mag mag	mag mag	, mag	mag	mag	mag	sp. type	mag	рс
894	4 19 12.7	+58 06 06	18.13	2.04	: 0.90	0.29	0.99	1.47	g0 V:	1.78	2570
895	4 19 12.8	+58 03 32	18.20	2.03	: 0.98	0.32	0.91	1.38:	f9 V-III		2750
896	4 19 12.9	+58 12 52	16.70 3.86:			0.37			g4 IV	1.76	2480
897	4 19 13.0	+58 19 26	17.66	3.13: 2.14		0.41			10717	1 40	0200
898	4 19 13.1	+58 18 05	16.75 4.23	3.47 2.48		0.43			k0 IV		2790
899	4 19 13.1	+58 06 15	17.49	2.2		$0.35 \\ 0.48$			g3 III k0.5 III	1.38	2280
900	4 19 13.3	+58 16 05	14.56 5.16 16.97 3.76:	4.28 3.03 3.03 2.13					g4 IV		3040
901	4 19 13.3 4 19 13.4		15.37 4.64	3.81 2.72		0.45		1.70	g-11	1.05	0040
902 903	4 19 13.4		18.31 3.69	2.80:: 2.13					f7 V-III:	2.13	2950
904	4 19 13.4	+58 16 30	18.05	2.64: 1.86					f2 V-III		4050
905	4 19 13.4	+58 11 58	13.96 3.44	2.60 1.73	0.83	0.31	0.72	1.10	a9 V	2.03	740
906	4 19 13.5	+58 13 08	17.67 3.63:	: 2.96: 2.03					a6 IV::		4730
907	4 19 13.5	+58 11 20	17.47 3.60	2.71 1.83					a9 V		3300
908	4 19 13.6	+58 19 28	16.88 3.42	2.56 1.5		0.28			a5 V		4250
909	4 19 13.7	+58 15 49	12.45 3.44	2.50 1.49		0.26			a3 IV		820 4100
910	4 19 13.7	+58 12 28	17.83 3.50	2.68: 1.80 2.98: 2.19		0.29					2360
911 912	4 19 13.7 4 19 13.7	+58 25 29 +58 14 24	17.80: 15.94 3.74	2.72 1.73		0.34	. 0.71	1.11	a5 V-IV		2280
913	4 19 13.8	+58 23 45	16.81 3.66:				0.88		20 / 2/	2100	
914	4 19 13.8	+58 10 08	17.90 3.58	2.00			0.84				
915	4 19 13.9	+58 11 52	16.47	3.1					k7 V:	0.96	316
916	4 19 13.9	+58 17 23	16.62 3.75	2.78 1.73	0.81				a4 V		3280
917	4 19 14.1	$+58\ 15\ 21$	16.19 3.68	2.73 1.68					a4 V-IV		2800
918	4 19 14.2	+58 16 35	16.83 3.63	2.63 1.60					a5 V-III		3740
919	4 19 14.2	+58 13 10	16.74 3.69:				0.66				3600
920	4 19 14.3	+58 21 07	17.68 3.63	2.72: 1.78		0.31			a7 V a3 IV		4310 4170
921	4 19 14.4	+58 10 32 +58 20 22	16.35 3.68	2.70 1.65 2.54 1.79		0.32			f4 IV		2860
922 923	4 19 14.6 4 19 14.6	+58 20 22	16.43 3.35 15.54 3.35	2.57 1.73		0.31			ñν		1420
923	4 19 14.0	+58 03 05	14.89 3.05	2.15 1.33		0.27			ь9 V		2850
925	4 19 15.0	+58 18 03	16.18 3.12	2.25 1.3					a0 V		5070
926	4 19 15.0	+58 17 49	17.56 3.48	2.70 1.74		0.31	0.71	1.08	a8 V-IV	2.12	4120
927	4 19 15.0	+58 13 05	17.43: 3.62	2.73 1.7					a7 V		3830
928	4 19 15.1	+58 26 16	17.41	2.40					: k0.7 V	1.67	870
929	4 19 15.3	+58 24 46	15.17 6.00:				1.31		037.111	0.75	4000
930	4 19 15.4	+58 15 00	17.20	2.87 1.82		0.32	0.75	1.17	a3 V-III f2 V		4080 278
931	4 19 15.4	+58 05 00 +58 04 19	11.47 2.93 17.52	2.27 1.53 1.93				1 20	f9 V-III		2240
932 933	4 19 15.6 4 19 15.6	+58 27 19	18.07:	2.45:: 1.7							4290
934	4 19 15.6	+58 09 52	17.41 3.53	2.71 1.80			0.80				3160
935	4 19 15.7	+58 12 20	17.97 3.51	2.68: 1.99					f5 V		3020
936	4 19 15.7	+58 24 39	16.44 3.44	2.61 1.78		0.32	0.79	1.21	f1 V		2060
937	4 19 16.0	$+58\ 15\ 04$	15.96 3.57	2.77 1.98		0.36	0.85	1.31	f5 IV		1910
938	4 19 16.4	+58 22 23	17.53 3.32:			0.29	0.54	0.86	a5 V		6150
939	4 19 16.5	+58 08 45	15.02 3.55	2.92 2.08					g5.5 IV	1.17	1470
940	4 19 16.5	+58 14 55	17.87 3.70	1.83			0.69	1.23	1-1 0 117	1 00	9170
941	4 19 16.5	+58 20 51	15.01 5.18	4.35 3.03		0.51	0.83		kl.2III		3170 1950
942	4 19 16.6 4 19 16.6	+58 19 27 +58 17 52	16.49 3.45 16.45 3.21	2.66 1.8° 2.45 1.46		0.33			a4 V:		4330
943 944	4 19 16.6	+58 17 52	17.06 4.84	2.40 1.40		0.47			g5.5 III		5430
944	4 19 16.7	+58 13 29	17.80 4.36	2.5		0.50			k1.2 V		930
946	4 19 16.7	+58 05 44	16.91	2.60: 1.5					a3 V-III		4510
947	4 19 16.8	+58 10 13	15.50 3.40	2.68 1.89		0.33			f6 IV		1710
948	4 19 16.9	+58 13 16	15.41 3.70	2.69 1.67		0.30	0.71	1.11	a4 IV	2.34	2480
949	4 19 16.9	+58 08 25	16.92 3.58:			0.24			a3 V-III		4730
950	4 19 16.9	+58 11 29	18.02: 3.55	2.58: 1.84		0.27			a8 IV:	2.19	6490
951	4 19 17.0	+58 25 20	18.13		2: 0.88:	0.32:	1.00:	1.49:	: _ 		
952	4 19 17.0	+58 18 10	15.68 3.63	2.63 1.66		0.31	0.72	1.11	a5 IV		2730
953	4 19 17.3	+58 22 15	16.59 3.49	2.60 1.58		0.29			a4 V	2.09	3800
954	4 19 17.3	+58 20 22	17.99 3.51	1.6		0.27			-037	1.00	4100
955	4 19 18.0	+58 19 31	17.57 3.37	2.55 1.68		0.30		1.05	a9 V k4 III	1.89	4120 930
956 957	4 19 18.0 4 19 18.0	+58 15 14 +58 08 29		5.24 3.68 2.80 1.76				1.08	a3 V-III		4330
901	- 19 10.U	T00 00 20	11.12	2.00 1.10	, 0.02	0.20	3110	1.00		2.01	2000

Table 3. Continued

1.9	ipie 3. C	ontinued											
No.	BA(2000)	DEC(2000)	v	U-V	P-V	X-V	Y-V	Z-V	V-S	V-I	Photom.	A_V	d
	hm s	0 / //										mag	\mathbf{pc}
												0.04	820
958	4 19 18.0	+58 28 46	17.86:		4.00	2.72:					k0.7 V k1 III	2.24	3340
959 960	4 19 18.1 4 19 18.2		15.17	3.72	9.78	1.75					a5 V		3900
961	4 19 18.2	+58 17 00	18.10		2.74::		0.93				40 1	2.00	0000
962	4 19 18.2		17.52		3.42:						k0 IV:	1,06	4700
963	4 19 18.3		16.06		2.60					0.05	4 5 5 75 5	2.10	2970
964	4 19 18.4		15.86		3.53	2.54	1.17	0.43	1.08	1.67	g4 IV	2.48	1210
965	4 19 18.7		16.83		2.66	1.71	0.84	0.29	0.69	1.08	84 V-IV g4 IV a8 III a9 V	2.04	5380
966	4 19 18.9		17.35	3.69	2.79	1.85	0.92	0.32	0.81	1.32	a9 V	2.41	2950
967	4 19 18.9	+58 27 53	17.97 15.39	2 20	0.64	2.10:	1.08:	0.44	0.80:	1.25	fe TV	1 70	1680
968 969	4 19 18.9 4 19 18.9		18.51	3.39	2.04	1.00	0.00	0.32	0.79	1.26	f6 IV g3 V f4 IV	1.19	3290
970	4 19 19.0			3.46	2.66	1.91	0.91	0.33	0.86	1.28	f4 IV	1.94	1070
971	4 19 19.1	+58 16 14	16.57	3.93::	2.86:	1.79:	0.92	0.36	0.94	1.66:	a0.5 V-III:	3.17	3230
972	4 19 19.2		17.88		3.02:	2.15:	1.01:	0.47:	0.88:	1.40			1640
973	4 19 19.2	+58 18 55	18.23	3.40	2.66:	1.91	0.89	0.35	0.79	1.21	f8 IV	1.59	6120
974	4 19 19.2	+58 12 45	16.30	3.62	2.68	1.59	0.78	0.28	0.63	1.01	a3 IV	2.26	4250
975	4 19 19.3	+58 28 44	17.85		0.67.	2.06:	0.85:	0.34:	0.95:	1.41	g8 V	1.30	3150
976 977	4 19 19.5 4 19 19.5	+58 12 29 +58 08 29	17 70		2.07:	2.57	ບ.ວນ 1 07	0.54	1 03	1.44	181V a3 IV g8 V g1 V k1 V f2 III	1.78	920
978	4 19 19.5	+58 15 41	15.03	3.42	2.62	1.80	0.88	0.32	0.77	1.16	fiV	2.01	1080
979	4 19 19.5	+58 10 32	17.00	3.50:	2.79	2.03	0.98	0.33	0.91	1.38	f9 V	1.80	1620
980	4 19 19.6	+58 10 50	17.58	3.62	$\frac{2.66}{2.73}$	1.80	0.87	0.32	0.72	1.13	f2 III	1.81	6520
981	4 19 19.7	+98 11 31	16.89	3.62	2.73	1.65	0.70	0.29	0.00	1.00	84 Y-111	2.29	9990
982	4 19 19.7		17.27	3.61	2.80	1.99							2320
983	4 19 19.9	+58 15 34	17.61	0.05	2.88		1.04		0.93				2180 3150
984 985	4 19 20.3 4 19 20.4		17.35 17.74		3.17:	9 14	1.03 1.01	0.40	0.87	7.40	an 137	1.84	4170
986	4 19 20.4	+58 03 38	15.46		2.81	2.01	0.96	0.36	0.85	1.30	f6 IV a3 IV	2.02	1490
987	4 19 20.5	+58 16 32				1.67	0.81	0.29	0.66	1.04	a3 IV	2.42	4270
988	4 19 20.5		15.95		2.45	1.61	0.81	0.28	0.74	1.13			
989	4 19 20.8		16.57		2.74		0.85		0.70	1.12	a4 V	2.44	3200
990	4 19 21.0		15.64				0.88		0.81		CT TIY.	1 44	2210
991	4 19 21.0	+58 14 28					$0.91 \\ 0.96$		0.81	1.23	f7 III: g5.5 IV		3310
992 993	4 19 21.1 4 19 21.2	+58 21 03 +58 04 53							0.09	1.40:	g3.5 IV	1.36	2850
994	4 19 21.2	+58 04 23	17.74	3.81			0.92				f2 V-III	2.14	3300
995	4 19 21.3	+58 15 43	17.81	3.81		2.21					f9.5 IV		3870
996	4 19 21.4	+58 04 20	17.74			1.59		0.29			a5 V		6160
997	4 19 21.4			3.45				0.29	0.63	1.01	a5 V		4610
998	4 19 21.5	+58 16 19		4.05		2.41	1.06	0.46	0.97	1.48	k0 V		1170
999 1000	4 19 21.8 4 19 22.0	+58 09 23 +58 22 03	16.92		3.69:		1.24 1.33	0.48	1.08	2.71			1950 286
1000	4 19 22.0		15.90	3.44	2.78			0.74	0.82	1.26	g1.5 IV		2180
1002	4 19 22.2		12.64		2.43	1.40	0.65	0.26	0.52	0.74		1.70	740
1003	4 19 22.4		17.74		2.60:	1.73	0.90	0.29	0.72	1.16	20 V	2.09	4070
1004	4 19 22.5	+58 17 19	16.66		2.70	1.65	0.82	0.31	0.68	1.08	a4 IV		4510
1005	4 19 22.6	+58 03 36					0.99		0.97	1.51	g0 V-IV		1790
1006	4 19 22.7	+58 21 00				1.93		0.33			f8 IV		3280
1007	4 19 22.7	+58 11 39			2.77		$0.83 \\ 1.27$				a5 V-III		3720 2740
1008 1009	4 19 22.7 4 19 22.8		14.60 17.21		4.31 2.60	1.69			1.10	1.07	k1.2 III a7 V		3840
1010	4 19 23.0	+58 26 50	18.19	J.U1			0.98:					2.00	2010
1011	4 19 23.0	+58 16 59	16.39	4.63:	3.65		1.24	0.46	1.07	1.74			
1012	4 19 23.1	+58 20 04	17.88	3.61	3.03:	2.13	0.97	0.38	0.87	1.34	g4 IV		4890
1013	4 19 23.2	+58 12 10	18.20				0.94	0.40	0.80	1.26	f3 V-III		3880
1014	4 19 23.3	+58 19 15	15.39		2.52		0.84				f6 IV		1860
1015	4 19 23.4	+58 19 40	17.43	3.59	2.64		0.85 1.20		0.69	1.08	a8 V		3750 1890
1016 1017	4 19 23.6 4 19 23.6	+58 17 02 +58 05 21	16.49 12.55	2 02	3.76 2.27		0.70		0.65	0.90	g9.5 IV	1.25	457
1017	4 19 23.0	+58 07 46			4.41		1.27		1.15		*	1.20	-201
1019	4 19 23.9	+58 15 06	15.89		3.69		1.18		1.06	1.65	g6 III	1.93	4160
1020	4 19 24.0	+58 09 39				1.61	0.77	0.28			g6 III a4 V-IV		3430
1021	4 19 24.1	+58 13 50					1.07	0.36					

Table 3. Continued

No.	RA(2000)	DEC(2000)	V U -	V P-V	VX-V	Y-V	Z - V	V– S	V~I	Photom.	A_V	d
	hm s	a <i>ì </i>	mag ma	g mag	mag	mag	mag	mag	mag	sp. type	mag	рс
		****					-		•			
1022	4 19 24.2		17.81 3.5		2.05	0.96	0.34			g0 IV	1.66	4680
1023	4 19 24.2		18.43		: 1.69:			0.72	1.21			
1024	4 19 24.3		16.06 3.4	1 2.57	1.75	0.85	0.34	0.73	1.13	f0 V g3 V		1880
1025	4 19 24.3		17.36	- 0.00	2.10	0.94	0.35	0.94	1.41	g3 V		1590
1026	4 19 24.5		15.79 4.4	7 3.60	2.63	1.19	0.43	1.07	1.00	g6 III	1.94	3940
1027	4 19 24.6		18.01	0 0 60	1.83	1.05		1.07	1.04	gz.5 III	1.92	2260
1028	4 19 24.6 4 19 24.6		16.71 3.4 16.32 3.6		1.63	0.93 0.79	0.31			fl V a4 V-IV		3160
1029 1030	4 19 24.0		17.89 3.3		: 1.90	0.90				g0IV	1.35	
1031	4 19 24.7		17.40		: 1.68	0.83	0.33			fi V-IV	1.75	
1032	4 19 24.7		16.22		1.89	0.91				ßΥ	2.03	
1033	4 19 24.7		16.32 3.6	6 2.69	1.79	0.87				fi III	1.92	
1034	4 19 24.9		18.04 3.4			0.92				: f3 V	1.99	
1035	4 19 25.0		12.71 6.7		4.13	1.64	0.74			k5.5 III		
1036	4 19 25.1		15.70 3.6		1.71	0.79	0.30			a6 V		
1037	4 19 25.1		18.27:		1.84:	0.91:	0.36:	0.85:	1.26	:		
1038	4 19 25.1	+58 11 14	14.56 3.1	7 - 2.49	1.74	0.83	0.31	0.74	1.08	f6 IV g5 III	1.41	1310
1039	4 19 25.4		16.87	3.54	: 2.54	1.13	0.41	1.09	1.69	g5 III	1.88	6550
1040	4 19 25.4		16.65		2.95	1.29	0.48	1.18	1.85	g8.5 III	2.31	5190
1041	4 19 25.5		18.02 3.4			0.94		0.77				
1042	4 19 25.6		15.08 4.1		2.36	1.05	0.40		1.51			
1043	4 19 25.9		16.45 3.6	1 2.63	1.60	0.80	0.29	0.63	1.01	a1.5 V a4 IV	2.44	
1044	4 19 26.0		15.69 3.6		1.61	0.79	0.29	0.66	1.00	a41V	2.18	3040
1045	4 19 26.2		17.99 3.5	0 2.03	1.75	0.90		0.79				
1046 1047	4 19 26.2 4 19 26.3		17.59 18.00	2.19	1.90	1.07 1.03		0.82		f2 V-III	2.50	0170
1048	4 19 26.5		18.36	2.09	2.01	0.87	0.36			12 V-111	1.12	
1049	4 19 26.6		17.92		1.88	0.82	0.30		1.05	grv	1.12	241(
1050	4 19 26.6		16.47 2.9	6 2 19	1.00	0.61	0.24			a1.5 V	1.59	5710
1051	4 19 26.7		14.99	o. _ o	3.85	1.53	0.64			k4 III	2.20	
1052	4 19 26.7		17.68	2.56	: 1.70	0.82	0.28			a9 V-III	2.04	
1053	4 19 26.7		16.87 3.4	3: 2.59	1.77	0.85	0.32			f5 III	1.55	
1054	4 19 26.9		14.50 5.0			1.29	0.49			k0 III	2.10	
1055	4 19 27.0	+58 24 06	18.25		1.95:	1.01:	0.32:	0.95:	1.43:	f2:	2.36	
1056	4 19 27.0	+58 08 56	18.36			0.88	0.30			f2 V-III	1.93	4860
1057	4 19 27.0		18.19			1.01	0.40	1.05	1.61	g5.5 V	1.97	1690
1058	4 19 27.3		17.41 3.4			0.95	0.37	0.79	1.27	f5 IV	1.88	4050
1059	4 19 27.4		15.37		2.98	1.26	0.50	1.15	1.83	k1 III	1.79	3760
1060	4 19 27.4		16.59 3.4		1.65	0.81	0.31	0.69	1.08	a7 V	2.08	2900
1061	4 19 27.6		15.61 4.4		2.55	1.17	0.43	1.06	1.64	g6 111	1.83	3830
1062	4 19 27.9		17.53 3.5		1.63	0.82	0.30	0.69	1.07	a71V	2.01	6090
1063	4 19 27.9		15.80 3.5		1.74 1.46	0.85	0.31	0.72	1.08	g5.5 v f5 IV k1 III a7 V g6 III a7 IV a7 V g4 V g5 III	2.22	1880
1064 1065	4 19 28.1 4 19 28.2		11.17 2.6 18.26 4.0			$0.61 \\ 1.05$	0.24	0.02	1 96	g4 V	0.13	170
1066	4 19 28.2		18.20 4.0 17.19 3.5		1.99	1.03	0.40	0.80	1.35	g5 III f4 V	2.14	2210
1067	4 19 28.4		15.78 4.3		2.58	1.17	0.44	1.04	1.67	f4 V g5 III f1 V	1 05	3860
1068	4 19 28.6		17.95 3.5		1.91	0.95	0.34	0.83	1.30	f1 V	2.27	3680
1069	4 19 28.6		15.88 3.4		1.80		0.33	0.79	1.24	ťΩV	2.12	1630
1070	4 19 28.9		16.23 3.3		1.71	0.85	0.30	0.74	1.14	f0 V f1 V f0 V	1.83	
1071	4 19 28.9		17.50 3.4		1.83		0.34	0.81	1.28	f0 V	2.21	
1072	4 19 29.0		17.28							a8 V-III		
1073	4 19 29.0		17.82 3.5	3 2.67		0.98	0.35	0.88	1.37			
1074	4 19 29.0		17.08 4.2	3.60:	2.54	1.12	0.44		1.58	g9.5 IV	1.64	2940
1075	4 19 29.0		18.32		2.30:		0.44	0.91	1.44	ki V	1.22	
1076	4 19 29.4		17.03 3.5	2.68	1.64					a4 V-III	2.22	
1077	4 19 29.6		17.76		3.05:					m2 V	0.57	
1078	4 19 29.6		18.22 3.3		1.94:			0.87	1.34	g0 V	1.52	
1079	4 19 29.9	+58 12 28 .				0.86	0.30	0.76	1.17	f0 IV	2.09	
1080	4 19 30.0		15.19 4.5	3.78		1.19	0.44	1.06	1.69	g8 III	1.82	
1081	4 19 30.0		18.01		2.09:		0.33	0.94	1.42	g0 V-IV	1.81	2400
1082	4 19 30.2		18.19		1.85:	0.86:				f9.5 V-III		
1083	4 19 30.3	+58 21 01 1	16.58 2.88	2.13	1.30	0.62	0.26				1.17	
1084	4 19 30.4		16.77 3.53				0.29				2.17	
1085	4 19 30.4	+58 24 05 1	10.01	2.81:	1.77	0.82:	0.28	0.83	1.25	a3 V-III:	2.68	Ե120

Table 3. Continued

Ta	rpre 9. (OTIFI	mm	ea											
No.	RA(2000)	DEC	(20	00)	V	U-V	P-V	X-V	Y-V	Z– V	$V \neg S$	V-I	Photom.	A_V	d
	hm s	0		"			mag	mag	mag	mag	mag	mag	sp. type	mag	pc
1000	4 10 20 5	1 50	1.4	10	10.00	0.61	0.60	1 61	0.79	0.20	0.63	1.01	54 W	2.10	3260
1086 1087	4 19 30.5 4 19 30.5	+58 +58			16.36 18.18	3.61	2.62		0.78				g2.5 III	0.15	3200
1088	4 19 30.5	+58				4.34	3 54						g4 IV	2.49	880
1089	4 19 30.6	+58		39	17.85	3.01	2.27:	1.42					f4 III	0.90	
1090	4 19 30.7				17.97			0.01	1.00	0.14	0.00	1 44	-717	1.78	1480
1091	4 19 31.2	+58	16		16.53		2.69	1.81	0.90	0.33	0.80	1.25	a9 V		2160
1092	4 19 31.4	+58			15.79		2.64	1,00	0.00	0.29	0.10	1.01	a5 V-IV	2.18	2300
1093	4 19 31.7				16.12		3.60		1.17		1.05		0.777		0070
1094	4 19 31.7				17.33		0.55	2.59	1.17					$\frac{2.19}{2.13}$	
1095 1096	4 19 31.8 4 19 31.9	+58 +58			15.88 15.26		$\frac{2.57}{2.46}$	1.69	0.75				62 IV	1.59	1880
1097	4 19 31.9				17.24		2.54		0.87	0.31	0.80	1.19	f4 V	1.59 1.75	2710
1098	4 19 31.9	+58			15.89	0.25	3.76			0.57	1.34	2.18	m2 V:	1.75 0.02	156
1099	4 19 31.9	+58			16.99	3.45	2.60		0.77			1.01	EW Y	4.00	7200
1100	4 19 32.0	+58	13	49	16.68	3.71:	2.71			0.27			a3 V-III		3700
1101	4 19 32.1	+58	26	42	18.30:			1.59:	0.69:	0.27:	0.60:	0.94:	g2.5	0.42	
1102	4 19 32.1				18.16	3.65		2.03:	0.97	0.37	0.90	1.38:	f3 V g7 IV		3440
1103	4 19 32.1				12.15		3.31	2.36	1.06	0.40	0.96	1.43	g7 IV	1.67	
1104 1105	4 19 32.1 4 19 32.2	+58 +58			16.46 17.62		4.09: 2.63		1.29:	0.00	1.13	1.75	g9.5 III a6 V-III	2.07	
1106	4 19 32.2	+58				3.84							g4 IV		2390
1107	4 19 32.3	+58				4.70							g9.5 III		3030
1108	4 19 32.4	+58			17.65			1.70	0.85	0.29	0.83	1.25	f2 V-III		3700
1109	4 19 32.4				17.08	3.49	2.69		0.94	0.34	0.82	1.27	f2 V		2480
1110	4 19 32.5	+58									0.65	0.88	a2 V-III	2.22	6430
1111	4 19 32.6	+58				3.41			0.93		0.86	1.28	f9.5 V	1.61	2710
1112	4 19 32.7	+58		16	17.51	0.50	2.68:	1.99:		0.28	0.90	1.36	g0 V	1.54 2.09	2160
1113 1114	4 19 32.7 4 19 33.0				18.23 15.99	3.50	2.70	1.92	0.95	0.32	0.91	1.37	f4 V f0 III	2.09	304U 3250
1115	4 19 33.0	+58 +58			17.94		2.59:		0.93	0.32	0.74	1 22	b8 V	3.27	8570
1116	4 19 33.2					3.32				0.34	0.82	1.21	f6 V	1.70	1110
1117	4 19 33.3	+58			17.21		2.53		0.78	0.27	0.72	0.97	a8 V-III		
1118	4 19 33.3	+58			18.10				1.06:						
1119	4 19 33.4	+58	18	30		3.42:			0.96	0.38	0.79	1.26	f1 V g0 IV	2.17	3150
1120	4 19 33.5	+58				3.67:	2.92	2.05	1.00	0.41	0.83	1.33	g01V	1.75	2920
1121 1122	4 19 33.6 4 19 33.6	+58			17.72	3.51		1.97:							
1123	4 19 33.6	+58			17.32	3.31	2.60:	2.54	1 01	0.32	1.05	1.17	k2 2 V	1 43	770
1124	4 19 33.6	+58				3.99	3.22		1.02	0.39	1.01	1.55	k2.2 V g3 III	1.66	7190
1125	4 19 33.8	+58				3.51:			0.84:				8		, - • •
1126	4 19 34.1					~ - ~					0.00		a7 V	2.23	3300
1127	4 19 34.2	+58	17	51	17.58	3.41:	2.65	1.72	0.87	0.34	0.68	1.12	a7 V a8 V g7 III	2.14	4110
1128	4 19 34.3	+58	16	04	16.75	4.77	3.87:	2.80	1.26	0.48	1.12	1.78	g7 III	2.21	5520
1129	4 19 34.4	408	ΤO	UB	17.47	3.48	2.78	1.91	0.94	0.55	0.04	1.20			
1130	4 19 34.4 4 19 34.6	+58 +58			18.03 17.84	3.51	2.66:	1.93	0.84	0.35				2.29 0.81	
1131 1132	4 19 34.6	+58			15.01	3 91	2.44		0.82		0.73			1.66	
1133	4 19 34.7	+58			16.24			1.92	0.94					2.16	
1134	4 19 34.8	+58			18.11			2.42:					k0.7 V:		1180
1135	4 19 35.0	+58			16.09		2.53	1.77	0.89	0.35	0.77	1.26	f3 V	1.78	1690
1136	4 19 35.0	+58	06	07	17.19		2.65:	1.91	0.93	0.32	0.89	1.35	f4 V	2.02	
1137	4 19 35.3	+58	15	17	17.55		2.67	1.74	0.89					2.97	
1138	4 19 35.3	+58	18	11	16.61	3.64:	2.89	2.08	0.95				f9.5 IV	1.81	
1139	4 19 35.5	458	10	UU OA	14.14	3.04	2.37	1.62		0.29			IO V	1.39	820
$\frac{1140}{1141}$	4 19 35.9 4 19 36.1				17.95 18.16			2.06:					f7 V	1,96	2980
1142	4 19 36.2	+58				3.12			0.71	0.28	0.66	0.96	f7 V a9 V g9 III	1.57	
1143	4 19 36.3					4.58:			1.20	0.47	1.07	1.67	g9 III	1.64	
1144	4 19 36.6				18.00			1 77	0.92	0.31	0.84	1.13	J		
1145	4 19 36.8	+58				3.93	3.37	2.32	0.96	0.44	0.91	1.35	k1.7 V	1.12	640
1146	4 19 36.8	+58	15	22	14.22	3.65	2.67	1.68	0.80	0.30	0.68	1.05	a5 V	2.24	1090
1147	4 19 36.8				17.62		2.44:	1.72	0.86	0.29	0.82	1.24	f4 V	1.66	3350
1148	4 19 36.8				18.15		0 ==	2.07:	0.93	0.33	0.93	1.42	k1.7 V a5 V f4 V g3 V	1.60	2310
1149	4 19 37.3	+58	22	ΰl	17.74		2.75:	1.97	0.90:	0.30	0.88	1.36			

Table 3. Continued

Ta	ible 3. C	ontinuea										
No	TP 4 (2000)	DEC(2000)	v <i>U-V</i>	P-V	X-V	Y-V	Z– V	$V \vdash S$	V-I	Photom.	A_V	d
MÓ.	hm s	0 / //	mag mag	mag	mag	mag	mag	mag	mag	sp. type	mag	рc
	11 111 5											
1150	4 19 37.5		17.41		2.10:	0.97:				g1.5 V k3 III		1710 1080
1151	4 19 37.5	+58 23 28	12.95 6.04	5.08 2.54	1.60	$\frac{1.48}{0.77}$	$0.61 \\ 0.28$			a7 V-IV		3140
1152	4 19 37.6	+58 11 11	16.68 3.45 15.00 3.28		1.80	0.87	0.32			f6 IV		1470
1153	4 19 37.7	+58 06 06 +58 26 57	17.69	2.57:		0.82:		0.72:	1.09	a0 V-III		7460
1154 1155	4 19 38.2 4 19 38.2	+58 21 00	17.67 3.43	2.56		0.93	0.32	0.81				
1156	4 19 38.4	+58 09 03	14.09 3.02	2.42		0.75	0.28			g3 V	0.74	530
1157	4 19 38.5	+58 23 42	15.59 3.55		1.89	0.94		0.84				1270
1158	4 19 38.6	+58 14 55	17.58 3.59	2.67	1.74	0.84	0.31			a7 V	2.24	4230
1159	4 19 38.7	+58 07 53	18.42		1.85:			0.85		1-1 737	. 51	1100
1160	4 19 38.9	+58 20 02	14.97 4.70	3.97 2.61		1.16 0.89	$0.47 \\ 0.31$			k1 IV f1 V	1.51 2.06	1640
1161	4 19 39.1	+58 15 17 +58 14 51	15.98 3.47 18.22	2.01	1.67:		0.30	0.72		11 7	2.00	10-10
1162 1163	4 19 39.3 4 19 39.3	+58 23 25	17.96:							f2 V-III	2.28	3430
1164	4 19 39.3	+58 05 30	18.36:		1.77:	0.78:	0.27:	0.87	1.36	g0 V-III:	1.29	3580
1165	4 19 39.5	+58 04 01	17.96: 18.36: 15.88	2.81	1.99					f3 IV		1800
1166	4 19 39.6	$+58\ 19\ 41$	17.47 3.34	2.49	1.60	0.80	0.31	0.69	1.03	a8 V	1.89	4380
1167	4 19 39.7		17.31	2.69:	1.83	0.94:	0.38	0.85:	1.29		1.04	
1168	4 19 39.8	+58 04 14	17.47	0.00	1.71		0.34				1.64	
1169	4 19 39.9	+58 25 20 +58 09 07	17.66: 3.25:: 18.34	2.03:	1.72:	1.00	0.29:	1.01	1.24	k1 V	1.45	1440
1170 1171	4 19 40.2 4 19 40.5	+58 18 04	16.76 3.43	2.53	1.58		0.29	0.60	0.95	a5 V	1.95	
1172	4 19 40.5	+58 27 13	15.06 5.22:			1.29	0.52	1.19	1.85	k1.2 III		3110
1173	4 19 40.7	+58 23 35	16.92		2.81		0.50	1.13	1.80	g8 IV	2.54	1810
1174	4 19 40.7	+58 23 59	18.13	2.51:		0.85:	0.34:					
1175	4 19 41.1	+58 11 45	16.61 3.66	2.95	2.11	1.00	0.36	0.92	1.39	g0 IV	1.84	2480
1176	4 19 41.2	$+58\ 05\ 27$	17.99		2.14:			0.92			1 00	2070
1177	4 19 41.3	+58 18 28	17.93 3.39	2.65:	1.92	$0.93 \\ 1.27$	0.33	1.19		f6 V k0.5 III		3070 5870
1178	4 19 41.7 4 19 42.0	+58 10 32 +58 06 39	16.56 5.12 17.55		3.01 2.11:					g1.5 V		1800
1179 1180	4 19 42.0	+58 16 57	15.97 3.19	2.44	1.69	0.83				f2 V		1840
1181	4 19 42.3		17.15 3.35		1.90	0.94	0.35	0.84	1.32	g0 IV		3850
1182	4 19 42.3		15.34 3.22	2.65		0.83	0.32	0.80	1.16	g5 V	0.99	
1183	4 19 42.5	+58 16 54	17.46 3.37:		1.86	0.87	0.34	0.77	1.20	f6 IV		4450
1184	4 19 42.6	+58 24 15	16.60 3.25		1.64	0.82	0.27	0.78	1.13	f0 V f3 V		2600
1185	4 19 42.6		18.10:: 3.57 17.61	2.75:	2.86:	0.96	0.40	1.25	1.34	m2V	2.17 0.11	
1186	4 19 42.6 4 19 42.6	+58 09 10 +58 14 18	17.59 3.45	2.65	1.84	0.92		0.80	1.95	f2 V		3260
1187 1188	4 19 42.8	+58 18 02	13.38 2.88		1.63	0.71	0.27	0.68	0.01	σ2 V	0.59	
1189	4 19 43.1	+58 20 29	18.19		2.57:		0.54	1.07	1.63	k2.5 V	1.56	1060
1190	4 19 43.2	+58 10 18	16.17 3.35	2.48	1.53	0.73	0.26	0.68	0.97	a6 IV		3790
1191	4 19 43.3	+58 13 36	18.11 3.28		1.89	0.94	0.33			f6 V		3430
1192	4 19 43.4	+58 09 17	13.42 3.03		1.24	0.56	0.21	0.47	0.65	a3IV		1670
1193	4 19 43.6	+58 21 54	16.09 3.49		1.53	0.71 0.90				a3 IV		4200 2110
1194 1195	4 19 43.8 4 19 44.0	+58 08 41 +58 05 55	17.37 15.28 3.32	$\frac{2.60}{2.63}$	1.92	0.90	0.34			g0V f6IV		1590
1195	4 19 44.0	+58 24 35	15.68 4.68:	3.88		1.14	0.50			k0.7 IV:		1580
1197	4 19 44.0	+58 21 04	18.15 3.29	2.45:		0.86	0.33	0.78	1.24	f3 V:		4460
1198	4 19 44.1	+58 10 39	17.74 3.30	2.55	1 77	0.85	በ 31	0.82	1 16	f2 V	1.83	3810
1199	4 19 44.7	+58 12 31	17.63		3.16	1.19	0.67	1.30	1.96	k6 V g1.5 f3 V	1.42	
1200	4 19 44.8	+58 28 13	17.79		1.90:	0.90:	0.38:	0.80:	1.19:	g1.5	1.30	
1201	4 19 44.8		15.89 3.11	2.40	1.68	0.82	0.29	0.75	1.09	13 V		1730
1202	4 19 44.8	+58 24 49 +58 22 13	17.94: 16.06 3.51	2.42:						g5.5 V: a1.5 V	0.58 2.29	
1203 1204	4 19 45.0 4 19 45.2	+58 22 13	17.13 3.37:	2.59			0.32	0.82				2830
1204	4 19 45.2	+58 08 37	18.24				0.38			g2.5 III	1.92	
1206	4 19 45.3	+58 12 16	17.85	2.48:	1.80		0.31	0.83	1.27	f5 V	1.67	3440
1207	4 19 45.3	+58 17 56	18.00 3.32	2.56:	1.80	0.88	0.36	0.79	1.20	f3 V		4010
1208	4 19 45.6	+58 21 39	16.55 3.53:	2.96	2.09	0.95	0.40	0.88	1.31	g7V	1.30	960
1209	4 19 45.7	+58 08 37	18.29	0.01	1.82:		0.36	0.82	1.11:	:		0100
1210	4 19 45.8	+58 20 21	17.92	2.64:		0.97	0.37 0.38:	0.83		f5 V		3130 8010
1211 1212	4 19 46.0 4 19 46.0		18.26 16.96 3.62	2.60		0.79		0.76				3900
1212	4 19 46.0	+58 14 17			1.92							2340
-210									3			

Table 3. Continued

T'a	ble	3. C	onti	nued											
No.	RA(2	2000)	DEC	(2000)	\overline{v}	UV	P-V	<i>X-V</i>	Y-V	Z- V	<i>V~S</i>	V-I	Photom.	A_V	d
	h m	s	۰	1 11	mag	mag	mag	mag	mag	mag	mag	mag	sp. type	mag	рc
1214	4 10	46.2	-1.58	21.38	16.52	3 41	2 59	1.63	0.80	0.32	0.70	1.07	a7 V g0 V: a3 V-III a5 V g9.5 V k5.5 V	2.04	2850
1215	4 19	46.3	±58	08 18	18.09	:		1.79:	0.79	0.26	0.89	1.18:	g0 V:	1.26	3200
1216	4 19	46.5	+58	22 44	18.30			1.83:	0.93:	0.28	0.77:	1.25	a3 V-III	2.79	6630
1217	4 19	46.6	4.58	05 36	17.78	:		1.98:	0.97:	0.39	0.78	1.14:	a5 V	2.87	4190
1218	4 19	46.7	+58	21 51	17.07		3.11:	2.24	0.94	0.42	0.95	1.39	g9.5 V	1.31	980
1219	4 19	46.7	+58	24 43	15.44	4.56	3.94	2.75	0.99	0.63	1.06	1.50	k5.5 V	0.69	295
1220	4 19	46.8	+58	23 58	14.07	4.29	3.51	2.42	1.10	0.40	1.02	1.55	g9 V f3 V g6 IV f3 V f4 V f6 V 9.5 V f9 V-III f0 V-III g0 IV g0 V g0 V g0 V-III g7 IV		
1221	4 19	46.8	+58	05 19	17.64			2.38:	1.08	0.49	0.99	1.51	g9 V	1.79	1070
1222	4 19	47.1	+58	08 22	18.29			1.76:	0.79	0.31	0.89	1.10:			
1223	4 19	47.4	+58	18 09	17.62		2.52	1.60	0.81	0.33	0.70	1.09	en 1 !		0500
1224	4 19	47.4	+58	19 51	16.82	3.23	2.44	1.71	0.85	0.33	0.75	1.12	13 V	1.03	2030
1225	4 19	47.6	+58	22 48	17.03		3.21:	2.25	1.01	0.39	0.98	1.48	goiv	1.04	2910
1226	4 19	47.6	+58	08 45	17.65		2.55:	1.80	0.91	0.33	0.62	1.11	13 V	1.00	3300
1227	4 19	47.7	+58	22 25	17.80		2.61;	1.87	0.99	0.33	0.01	1.01	£4 V	9 13	3120
1228	4 19	47.8	+58	22 38	17.93		2.73:	1.97	0.91.	0.31	0.31.	1 22	6 V	1.68	2090
1229	4 19	48.0	4.00	00 10	17.94		2.59	1.00	0.30	0.37	0.75:	1.12	10 1	2.00	-000
1021	4 10	40.0	150	17 19	17.04	2 21.	2.65	1 01	0.00.	0.35	0.82	1.25	f9.5 V	1.47	2090
1000	4 10	40.0	1.58	25 30	17.75	0.01.	2.62	1 79.	0.87:	0.38	0.74:	1.12	f0 V	2.09	3900
1232	4 19	48.3	±58	11 30	18.13		2.02.	2.25:	1.01	0.44	0.96	1.49	g8.5 V	1.56	1560
1234	4 19	48.5	+58	21 05	18.34		2.45:	1.81:	0.87	0.32	0.81	1.25	f7 V-III	1.47	4060
1235	4 19	48.8	+-58	22 19	17.82		2.55:	1.71:	0.79:	0.27	0.81:	1.17	f0 V-III	1.95	4290
1236	4 19	49.0	+58	10 20	18.38			1.72:	0.87	0.30	0.78	1.19	f2 V-III	1.82	5160
1237	4 19	49.0	+58	12 02	16.57	3.53	2.84	2.01	0.95	0.35	0.86	1.30	g0 IV	1.62	2690
1238	4 19	49.0	+58	05 54	18.06			1.83:	0.82	0.27	0.89	1.27	: g0 V	1.30	3100
1239	4 19	49.3	+58	27 16	17.25	3.42:	2.50:	1.55	0.82:	0.30	0.65	1.02	a0 V	2.47	6550
1240	4 19	49.3	+58	23 11	17.10		3.25:	2.27	1.03	0.44	0.98	1.39	g8.5 V	1.64	940
1241	4 19	49.5	+58	08 45	18.09	,		2.40:	1.17	0.43	1.07	1.57	g0 V-III g7 IV	2.59	1740
1242	4 19	49.5	+58	06 58	15.36	3.72	3.08	2.10	0.94	0.37	0.88	1.25	g7 I V	1.19	1000
1243	4 19														
1244		49.6	+58	07 41	18.29			2.01:	0.94	0.40	0.79	1.10	f3 V f5 V f1 V-III f3 V g5.5 III:	1 40	5170
1245		49.7	+58	15 02	18.43			1.73:	0.84	0.33	0.00	1.20	: 13 V	1.03	3000
1246		49.8	+58	05 21	17.92		0.00	1.90:	1.02	0.34	0.04	1.30	10 V F1 V-111	2.56	2000
1247		49.9	+58	11 44	17.78	,	2,00;	1.00	0.80	0.30	0.00	1.04	f3 V	1.84	3200
1248 1249		50.0	+50	11 02	10 20	1	2.00.	2 27.	0.03	0.33	1.03	1.45	g5.5 III:	1.24	0200
1250		50.0	1-50	22 21	15 23	3 28	2.70	1 90	0.83	0.35	0.80	1.11	e6 IV	0.76	1930
1251		50.3	158	17 31	17.85	3.20	2.10	2.30	1.00	0.45	0.97	1.42	k0 V	1,46	1250
1252		50.3	+58	15 16	16.93		3.72:	2.67	1.08	0.55	1.06	1.63	k3 V	1.49	590
1253		50.3	+58	19 07	17.85	3.12:	2.58:	1.92	0.90	0.36	0.84	1.27	g3 V:	1.18	2440
1254		50.3	+58	23 18	16.04	4.39:	3.63	2.54	1.14	0.44	1.07	1.61	g9.51V	1.79	1700
1255		50.4	+58	16 27	18.06	1	2.63:	1.66:	0.83	0.35	0.65	1.03	a0.5 V	2.61	8310
1256		50.4	+58	13 40	17,68	i	2.64	1.82	0.84	0.29	0.83	1.26	f1 V-III	2.06	3590
1257		50.5	+58	17 35	15.67	3.67	3.11	2.13	0.86	0.41	0.86	1.20	k1.2 V	0.82	540
1258	4 19	50.6	+58	16 09	16.17	3.45	2.82	2.02	0.90	0.36	0.86	1.25	g5.5 III: g6 IV k0 V k3 V g3 V: g9.5 IV a0.5 V f1 V-III k1.2 V g5.5 V k3 V	1.26	920
1259	4 19	50.8	+58	10 20	15.63	3.94	3.41	2.35	0.90	0.44	0.94	1.32	k3 V	0.82	438
1260			+58	24 52	17.72	:	2.68:	1.97:	0.90:	0.42:	0.89	1.27	:	1 50	1800
1261		50.8	+58	15 08	16.36	3.29	2.54	1.81	0.87	0.31	0.84	1.26	14 V	1.76	1790
1262		50.8	+58	17 26	15.84	3.46	2.79	1.99	0.91	0.36	0.83	1.22	16 V 16 V 16 V 16 V 16 V 16 V 17 V 18 S S V	2.02	2020
1263		50.9	+58	05 04	17.97	,		1.84:	0.94	0.39	0.82	1.23	149 5 37	1.07	270
1264		50.9	+58	11 16	17,72		0.05	2.64	1.01	0.03	1.09	1.09	KO'A A	1.41	010
1265		51.1	+58	24 48	17.44	l 1	2.95	2.23	0.70	0.40	0.00	1.43			
1266		51.2	+-58	U5 56	17.62		0.60	1.07	0.79	0.30	0.74	1.12			
1267		51.3	+58	10 47	16.02	9 9 9 6 -	2.00	1.79	0.91	0.38	0.83	1 10	FG V	1 76	1940
1268		51.5	+58	07.04	17.00	. J.30:	2.04	1.91	0.92	0.30	0.02	1 28	f2 V	2 11	3530
1269		51.6	+58	07 14	14.60	7 2 0 5	2 20	1.00	0.53	0.34	0.60	0.20	f6 IV	1.06	1610
1270		52.2	+00	00 05	17.00	2.90	2.25	7.01	0.14	0.27	0.03	1.31	σ5.5 V	1.37	1610
1271		52.5	+00	17 44	10 00	, 2	2.07	1 02.	1.04	0.01	0.70	1.31	50.0	1.5.	
1272 1273		52.9 53.0	+20	US U.2	16.00	í	2.04	1 73	0.83	0.20	0.83	1.23			
1273		53.0	4-90	13 25	10.00	, R	4.70	1.87	0.92	0.32	0.85	1.32	•		
1274		53.3	工 50	05 22	17.79			1.61	0.79	0.31	0.69	1.05	f3	1.40	
1275	4 10	53.4	T-50	10 22	16.15	3.76	3.01	2.19	1.03	0.38	0.94	1.43	f9.5 IV f5 IV	2.03	1850
1277	4 10	53.6	158	26 53	16.93	2 3.66	2.82	2.04	1.01	0.41	0.86	1.29	f5 IV	2.18	2800
1411	- 10		, 50	_0 00	10.01	. 0.00.	2.02.						•		

Table 3. Continued

	able 5.	Commueu	L								
No.	RA(2000)	DEC(2000) V U-V	' P-1	/ X-V	′ Y-V	′ Z-V	v-3	V-I Photom	. Av	
	hm s	0 1 11							mag sp. type		
1050	4 10 50 0	150.00.50	10 10 0 15	0.50	1.50						
1278 1279				2.58	1.79	0.77 0.85			1.02 g6 V 1.32 g7 V	0.75	285
1280				2.50	: 1.48				1.07 a2 V-III		2490 7640
1281		+58 07 14				0.84			1.15 f3 V		1280
1282		+58 10 30			2.71	1 91	0.44	1 12	1 74 actii	9 12	4260
1283		+58 18 31	14.90 4.39	3.61	2.59	1.14	0.43	1.03	1.60 g6 III	1.82	2770
1284		+58 21 53		2,80		0.96	0.35	0.88	1.33		
1285		+58 24 59			2.58				1.47 k4.5 V:	0.81	720
1286		+58 14 41			1.88	0.88			1.20 g0 IV		3840
1287 1288		+58 15 42 +58 19 29			1.90 1.76	0.87 0.92			1.18 gl V	1.31	870
1289		+58 06 59			1.62	0.92			1.16 0.96 f9.5 IV	0.78	770
1290		+58 23 06			1.76	0.86			1.21 f1 V		770 1730
1291		+58 12 43		2.00	2.77		0.56		1.56 k3.5 V		680
1292		1 50 00 51	10 04		0.00	1.00	0.11		4 0 - 0	~	000
1293		+58 06 14	16.89	2.68	1.90	0.85	0.34	0.81	1.37 a6 1.17 g5.5 V 1.29 g1.5 V::	1.03	1430
1294		$+58\ 19\ 03$	18.27	2.31	: 1.84:	0.80:	0.33	0.83	1.29 g1.5 V::	1.00	3540
1295	4 19 56.0	+58 11 01	18.28		2.49:	1.03	0.49	1.08	1.58 k1.7 V	1.59	
1296		+58 19 19	18.28 17.97	2.35	1.53	0.72			0.98 a9 V		5740
1297 1298		+58 17 52	10.02 3.41;	2.48	1.48	1.01			0.93 a3 V-III	2.00	3330
1299		+58 17 52		3.07	2 94		0.40	1 21	1.23 1.88 g4 III:	2.92	1990
1300		+58 16 39	17.71		1.77			0.79	1.25 f2 V	1.86	
1301	4 19 56.4	+58 10 40	17.31 3.55:			0.74			0.90 a4 V	2.08	
1302		+58 21 51	17.46	2.65	: 1.92	0.97	0.37		1.27		
1303		+58 16 31	17.54 3.27:			0.90	0.34				
1304		+58 19 06		2.75			0.36		1.28 f4 V-IV:		
1305	4 19 56.6	+58 10 21	18.28						1.01 a3 V-III	2.28	8330
1306 1307	4 19 57.1 4 19 57.2	+58 26 10	17.77		1.75:						
1308	4 19 57.2	+58 16 48 +58 24 03	13.87 3.24 16.95 3.32:		1.73	U 00	0.31	0.76	1.12 f2V	1.74	670
1309	4 19 57.8	+58 17 19	16.46 3.51		1.85	0.00	0.25	0.70	1.23 f1 V	2.15	1060
1310	4 19 57.8	+58 23 42	18.00			0.79:	0.26:	0.77	1.08: a9	1.78	1500
1311	4 19 57.8		17.88						1.79 k0 IV	2.24	3230
1312	4 19 57.9	+58 16 03	16.98 3.19:	2.52	1.79	0.88	0.33	0.80	1.22 f6 V	1.55	
1313	4 19 58.2	+58 22 28	17.94						1.35 f3 V-III	2.48	
1314	4 19 58.2	+58 17 13	15.64 4.88:					1.11	1.75 g9.5 III	1.91	3980
1315 1316	4 19 58.5 4 19 58.7	+58 09 23 +58 06 39	16.67 3.39: 15.66 3.11		1.53					1.00	
1317	4 19 58.8	+58 06 58	15.62 2.59		1.12	0.74	0.20	0.51	1.02 a9 V	1.62	1940
1318	4 19 58.8	+58 10 02	18.56	1.04		0.92	0.23	0.01	1.74 o7 V	1.36	2370
1319	4 19 58.9	+58 20 24	16.86 3.40:	2.62	1.85	0.89	0.34	0.80	1.24 g7V 1.20 f3V	1.91	
1320	4 19 59.0	+58 17 21	17.71	2.57	1.81	0.93	0.37				
1321	4 19 59.1	+58 08 54	18.05		1.86:	0.92			1.28: f4 V-III		
1322	4 19 59.3		16.24		2.80	1.00	0.61		1.62 k5 V	0.93	
1323	4 19 59.3		17.39 3.25:			0.87			1.20 f6 V	1.57	
1324 1325	4 19 59.4 4 19 59.6	+58 10 58	17.65	2.62	1.79	0.86	0.34	0.72	1.05 f0 V-IV		
1326	4 19 59.6	+58 17 N2	16.52 3.36 16.85 3.50:	2.69	1.89	0.90	0.32	0.00	1.27 19 V 1.24 f5 III	1.59 1.65	
1327	4 19 59.8	+58 14 30	17.92	2.52	1.87	0.87	0.35	0.87	1.32 g3 V-III:		
1328	4 19 59.8		16.80 3.52		1.72		0.33	0.75	1.17 a9 IV	2.06	
1329	4 20 00.0	+58 15 58	17.28 3.33:	2.63	1.79	0.86	0.34	0.77	1.16 f1 V	1.98	
1330	4 20 00.4	+58 20 52	16.86 3.59:	2.67	1.64	0.79	0.33	0.66	0.98 a4V	2.26	
1331	4 20 00.5	+58 23 11	17.97		1.74	0.93:					
1332	4 20 00.6	+58 25 30	16.07 3.89		2.14				1.31 f0 V:	2.81	1300
1333 1334	4 20 00.7	+58 09 59	15.12 4.34	3.50	2.50	1.13	0.42	1.05	1.58		
1334	4 20 00.7 4 20 01.2		18.29 16.64	2 66.			0.31	0.69:	1.04 f8 1.44 k3.5 V 1.25 f2	1.12	ra^
1336	4 20 01.2		17.80	3.66:	1.91		0.53	1.00	1.44 k3.5 V 1.25 f2	1.05	580
1337	4 20 01.8		16.77 3.37:	2.59		0.30	0.33	0.04	1.25 f2 1.19 f1 V	2.20 1.99 2	2440
1338	4 20 01.8		17.86	00	1.87	0.92	0.33	0.84	1.25 f2 V-III	2.10	
1339	4 20 01.8		15.12 4.91:	4.08		1.24	0.47	1.12	1.72 k0.5 III	1.70 3	
1340	4 20 01.9	+58 21 27	17.64	2.75:	1.76	0.83	0.38	0.76:	1.20 a6 V	2.39	
1341	4 20 02.0	+58 26 19	13.15 3.23	2.53	1.71	0.79	0.33	0.69	0.98 fl V		520

Table 3. Continued

1.0	able o. (Jonethaea										
No.	RA(2000)	DEC(2000)	V $U-V$							Photom.	A_V	d
	hm s	0 / //	mag mag	mag	mag	mag	mag	mag	mag	sp. type	mag	рc
1342	4 20 02.1	+58 14 33	14.95 3.32	2.47	1.40	0.68	0.26	0.55	0.83	a1.5 V	2.02	2320
1343	4 20 02.1	+58 11 17			2.47	1.06	0.44	1.04	1.51	k0.7 V	1.69	690
1344	4 20 02.1		17.50 3.49	2.69	1.88	0.97	0.36	0.83	1.29	f2 V	2.15	
1345	4 20 02.6	+58 14 43	16.53		2.92	1.31	0.50			g8 III	2.33	4780
1346	4 20 02.6	+58 25 30	18.03:			0.95:						
1347	4 20 02.6	+58 14 04		2.26	1.28	0.67				a1.5 V	1.73	6666
1348	4 20 02.7	+58 10 16	16.49 3.95	3.09	2.21	1.06	0.38	1.00	1.49	f7 III	2.31	2720
1349	4 20 02.7	+58 17 58	16.96 3.52	2.90	2.04							
1350	4 20 03.2	+58 14 09	18.46		1.84:	0.98	0.37	0.78	1.30	ь9 V	3.36	8710
1351	4 20 03.3	+58 08 41	16.10 2.78	2.05	1.11	0.58	0.20	0.49				
1352	4 20 03.3	+58 12 22	18.17			1.01	0.35	0.87:				
1353	4 20 03.6	+58 25 26	16.93	3.10:	2.20	0.95	0.41			g8.5 V	1.42	96
1354	4 20 03.6	+58 13 47	17.50 3.25	2.65	1.90	0.97	0.37	0.84				
1355	4 20 03.7	+58 07 57	15.66 3.41	2.69	1.89	0.92				f6 IV	1.79	181
1356	4 20 04.0	+58 17 49	18.26		1.89:	0.93		0.87		!		
1357	4 20 04.1	+58 12 34	14.96 2.22	1.75	1.09	0.58	0.23	0.50				
1358	4 20 04.2	+58 10 26	17.38	2.54	1.62	0.78	0.31	0.68				
1359	4 20 04.2	+58 10 48	17.37		2.28	0.98	0.37	0.99				
1360	4 20 04.3	+58 11 37	17.38 17.37 18.32 18.05			0.85		0.78			1.74	
1361	4 20 04.4	+58 20 14				0.79:	0.41:	0.84:	1.23	g8.5 V:	0.63	
1362	4 20 04.6	+58 19 44	16.50 3.10			0.66	0.27	0.51	0.76	a1.5 V	1.72	545
1363	4 20 05.2	+58 21 11	17.86	2.55:	1.71	0.86	0.31	0.84:	1.21			
1364	4 20 05.4	+58 19 19	18.49		2.00:	0.89	0.41	0.86	1.27	g9 V	0.99	230
1365	4 20 05.6	+58 12 04	16.61 3.43	2.64			0.32	0.77	1.13	a9 V	2.09	243
1366	4 20 05.9	+58 11 41	15.96		3.01	1.29	0.49	1.19	1.87	k0 III	2.18	414
1367	4 20 05.9	+58 16 36	18.38		1.85	0.97	0.37	0.81	1.28	b9 V	3.40	825
1368	4 20 06.1		17.11 3.50	2.81:	2.04	0.95	0.36	0.94	1.37	g1.5 V	1.61	156
1369	4 20 06.2	+58 24 28	15.51 4.90	4.01:	2.75:	1.28				g9.5 III:	1.97	364
1370	4 20 06.8	+58 22 47	17.43		2.74:	1.16:	0.58	1.51	2.54	m1 V::	0.49	33
1371	4 20 06.9	+58 11 50	17.11 3.22	2.55	1.79	0.87	0.30	0.84	1.21	f7 IV	1.46	401
1372	4 20 07.4	+58 11 51	17.14 3.26	2.46	1.42	0.67	0.25	0.60	0.90	a3 IV	1.85	757
1373	4 20 07.5	+58 24 32				1.18:						
1374	4 20 07.5		16.36 3.45	2.81						g3 V	1.46	109
1375	4 20 07.8		15.91 3.68		1.64	0.83				a3 V-III	2.41	263
1376	4 20 08.4	+58 22 43			1.98:					f2 V-III	2.37	252
1377	4 20 08.6	+58 08 06	15.80	3.77	2.70	1.20	0.46	1.07	1.67	g7 III	1.95	401
1378	4 20 08.7	+58 20 49			2.87	1.33				g9.5 IV	2.53	158
1379	4 20 08.7	+58 15 06	17.53 3.29			0.85	0.32	0.71			1.93	381
1380	4 20 09.1	+58 16 39				0.91	0.36	0.81			1.71	
1381	4 20 09.2		16.49 3.12	2.26		0.76				b9.5 V	2.21	556
1382	4 20 09.8	+58 10 50			1.84	0.91	0.33			f5 V	1.70	
1383	4 20 09.9	+58 13 10				0.64				a5 V-III	1.31	
1384		+58 17 42	18.24		2.09:	0.93					1.25	198
1385	4 20 10.3	+58 19 40	17.17:	2.63:	1.55:	0.80	0.29:	0.76:	:1.23	a1.5 V-III		
1386	4 20 10.4		15.60 3.84							k0.5 IV	0.57	
1387	4 20 10.7		15.68 3.74							a3 V-III	2.53	
1388	4 20 10.9	+58 15 32		· -		0.82				k0.5 V	0.74	
1389		+58 09 00				0.99	0.32	0.81				
1390		+58 17 31		2.70	1.70		0.33			a5 V-III	2.26	417
1391	4 20 11.0	+58 13 49			2.11	1.01	0.39	0.90				
1392	4 20 11.1		17.37 3.31				0.30	0.77		f0 V	1.96	348
1393	4 20 11.5	+58 10 11	16.82 3.34			0.71	0.26			a6 V	1.82	
1394	4 20 11.5	+58 16 58	16.11 3.41		1.45	0.70	0.25			a3 IV	1.98	
1395	4 20 11.9	+58 15 45	15.24 3.15		1.61	0.80	0.29	0.67		f3 III:	1.25	
1396	4 20 12.2	+58 08 52	17.65	~20	2.12	1.02			1.45			
1397	4 20 12.8	+58 21 12	15.72 3.50	2 80	1.98	0.94				f9.5 IV	1.63	183
1398	4 20 12.8		17.04 3.72		1.72	0.84				a4 V-III	2.44	
1399	4 20 13.2		17.75	2.10		0.96	0.36	0.85			2.17	
1400	4 20 13.2		14.74 4.67	3 20	2.72	1.22	0.30			g9.5 III	1.67	
1400	4 20 13.3	+58 22 40								f9 IV	1.98	
								0.50	1.41	fi V	2.14	
1402	4 20 14.4	+58 18 31			1.86	0.91	0.36	0.75	1.21	11 V b9.5 V	2.14	
1403		+58 16 38	17.66	2.61	1.69	0.87				V 6.60	2.09	090
1404					2.00	1.01		0.80				
1405	4 20 14.4	+58 15 11	17.05 3.49	2.60	1.83	0.89	0.35	0.80	1.21			

Table 3. Continued

No.	RA	(20	100)	DEC	(20	000)	V	U-V	P– V	X-V	Y-V	Z-V	V-S	V-I	Photom.	A_V	d
	h n	1	5	•	1	"	mag	mag	mag	mag	mag	mag	mag	mag	sp. type	mag	
1406				+58	15	56	18.36			1.93:	0.85	0.36	0.86	1.26	g7 V	1.03	2500
1407	42	0 1	4.7	+58	21	15	16.97		2.82						a5 V-III		3310
1408			4.9				17.21			2.10	0.95	0.37	0.89	1.31:	g5 V		1370
1409			4.9				15.88	3.36	2.51	1.52	0.71	0.28	0.65	0.94	a5 V-III	1.88	2760
1410			5.4				17.18			2.24	1.00	0.42	0.90	1.29	g8.5 V		1050
1411			5.5				16.29	3.42:	2.53	1.50	0.71	0.29	0.58	0.90	a1.5 V		4020
1412	4 2	0 1	5.8	+58	14	44	18.33			1.87:	0.85:	0.31:	0.89:	1.28:	g0 V-III	1.38	3390
1413			6.0				16.36	4.08:	3.64	2.53	0.91	0.59	0.94	1.38	k5 V	0.29	600
1414	4 2						17.14			2.84	1.21	0.51	1.19	1.84	k1.5 V	2.33	510
1415	4 2	0 1	6.8	+58	12	44	18.04			2.22:	1.01:	0.37:	0.93	1.36	g1.5 III	1.60	
1416	4 20	0 1	6.8	+58	10	57	15.27	3.67		2.13							1340
1417	4 20	31	7.6	+58	11	00	17.45								g7 V		1780
1418	4 20) 1	8.2	+58	11	36	14.37	3.24	2.38		0.64						2250
1419	4 20						17.86			1.72:						0.70	
1420	4 20) 1	9.9	+58	12	15	17.31	_	2.61:								2740

CHEMICAL COMPOSITION OF THE RS CVn-TYPE STAR LAMBDA ANDROMEDAE

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Abstract. Photospheric parameters and chemical composition are determined for the single-lined chromospherically active RS CVn-type star λ And (HD 222107). From the high resolution spectra obtained on the Nordic Optical Telescope, abundances of 22 chemical elements and isotopes, including such key elements as $^{12}\mathrm{C},~^{13}\mathrm{C},~\mathrm{N}$ and O, were investigated. The differential line analysis with the MARCS model atmospheres gives $T_{\mathrm{eff}}=4830~\mathrm{K},~\log g=2.8,~\mathrm{[Fe/H]}=-0.53,~\mathrm{[C/Fe]}=0.09,~\mathrm{[N/Fe]}=0.35,~\mathrm{[O/Fe]}=0.45,~\mathrm{C/N}=2.21,~^{12}\mathrm{C/^{13}C}=14.$ The $^{12}\mathrm{C/^{13}C}$ ratio for a star of the RS CVn-type is determined for the first time, and its low value gives a hint that extra-mixing processes may start acting in low-mass chromospherically active stars below the bump of the luminosity function of red giants.

Key words: stars: RS CVn binaries, abundances – stars: individual (λ And = HD 222107)

1. INTRODUCTION

The RS CVn-type stars have been studied thoroughly since 1965 when their peculiar light curves were detected (Rodonó 1965; Chisari & Lacona 1965) and a new distinct class of binaries was named (Olivier 1974; Hall 1976). RS CVn binary systems are typically composed of two late-type chromospherically active fast-rotating stars, at least one of which has already evolved off the main sequence (Hall 1976). Tidal forces between the close components make their rotational period to be equal to the orbital period. Similarly to other cool active stars, RS CVn-type variables are remarkable due to large starspots, strong chromospheric plages, coronal X-ray and microwave emissions, as well as strong flares in the optical, radio and other spectral regions. General properties of RS CVn systems are comprehensively described by Montesinos et al. (1988). The photometric brightness variation analysis, Doppler imaging and spectral line analysis of RS CVn stars indicate that starspots may cover more than 20% of their surfaces (Rodonó et al. 1995; Berdyugina et al. 1998b, 2000; Jeffers 2005; Alekseev & Kozhevnikova